

# Component Model of Ferroelectric Capacitors

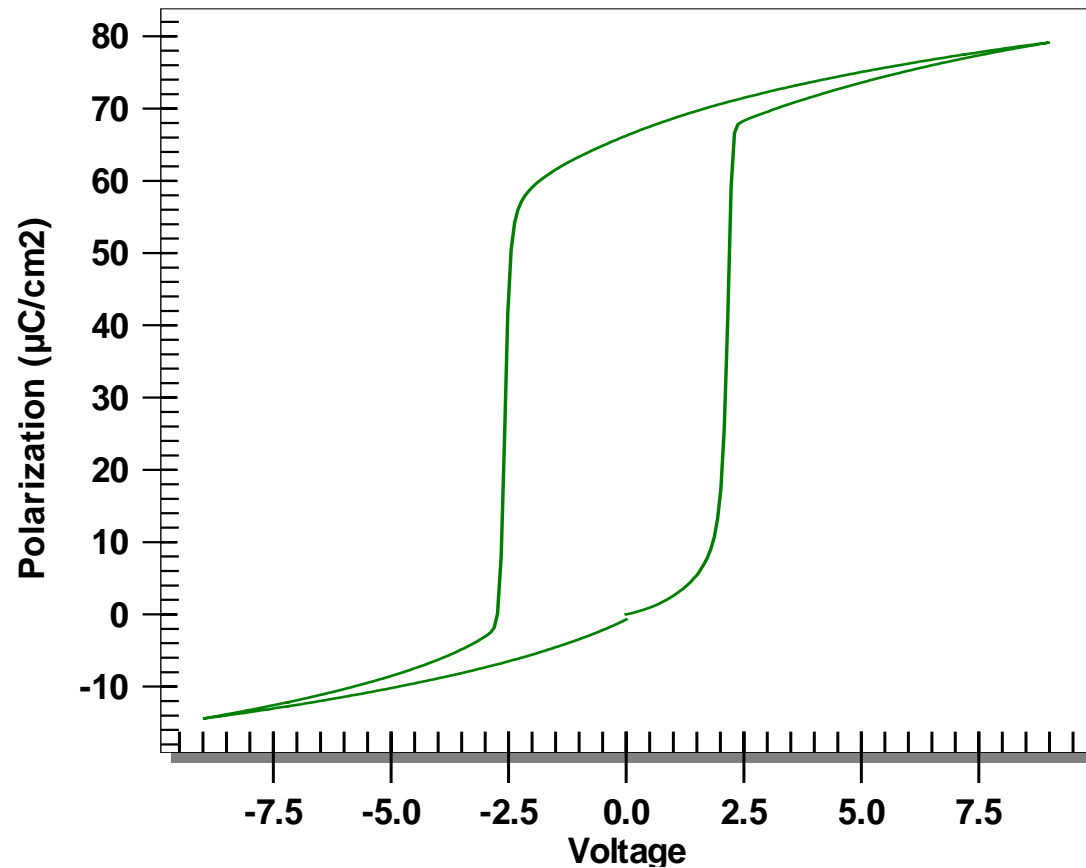
Joe T. Evans,  
*Radiant Technologies, Inc.*

*January 16, 2011*

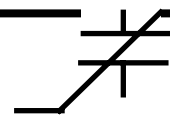
[www.ferrodevices.com](http://www.ferrodevices.com)



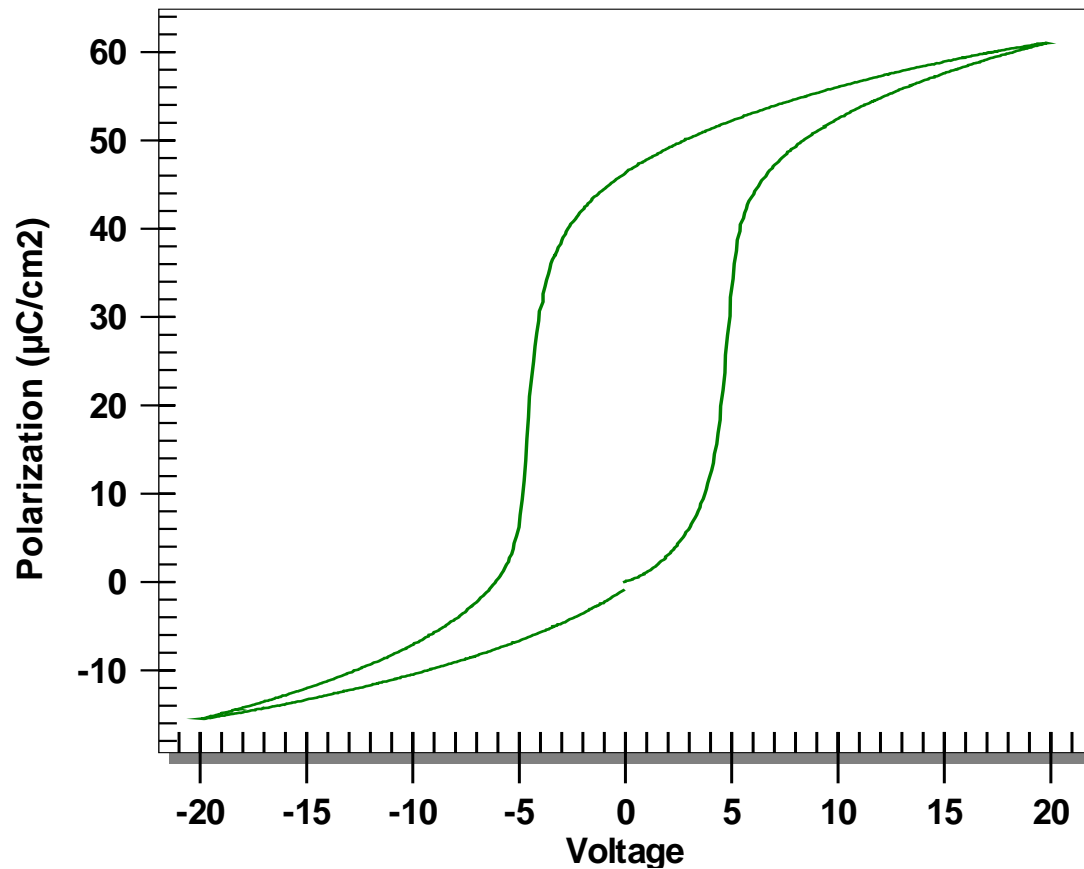
# An Excellent Hysteresis Loop



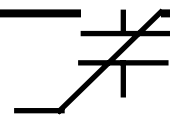
- This loop is nearly “perfect”. Most loops are not. After this presentation, you should be able to discern the difference upon inspection.



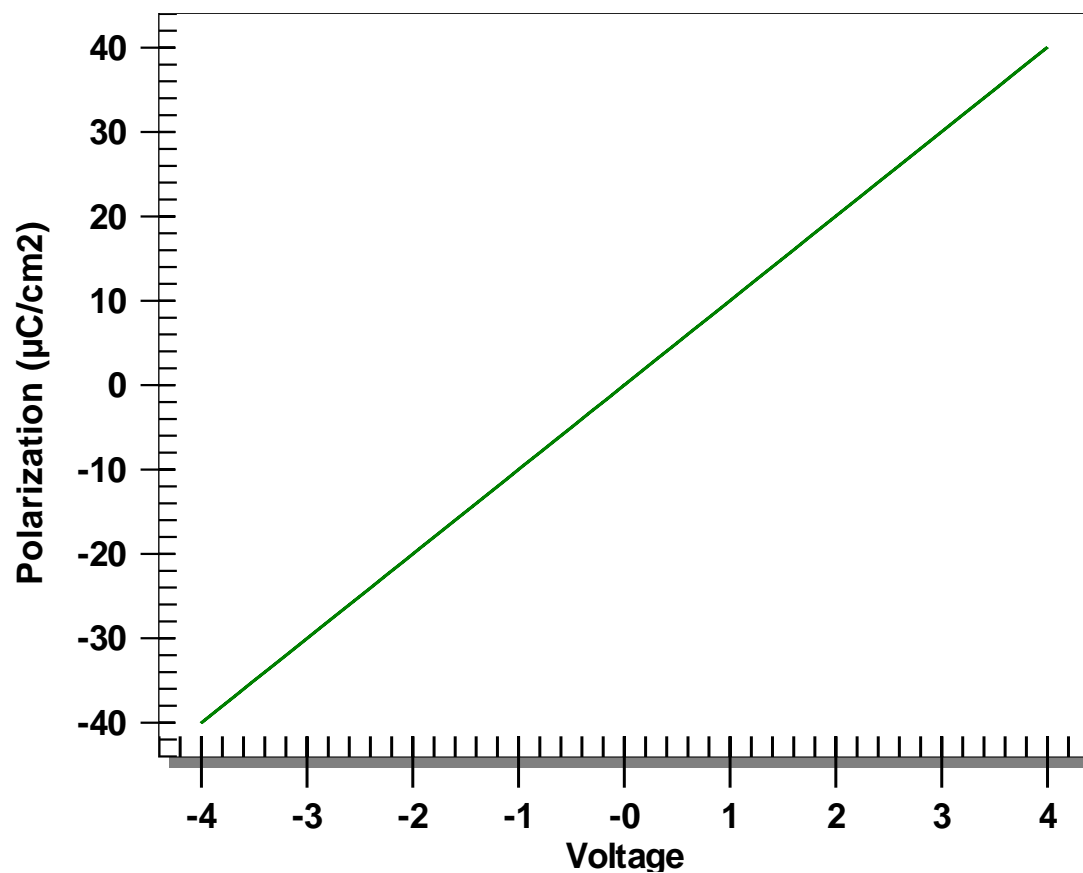
# What is this?



- Is this loop as good as the previous loop?

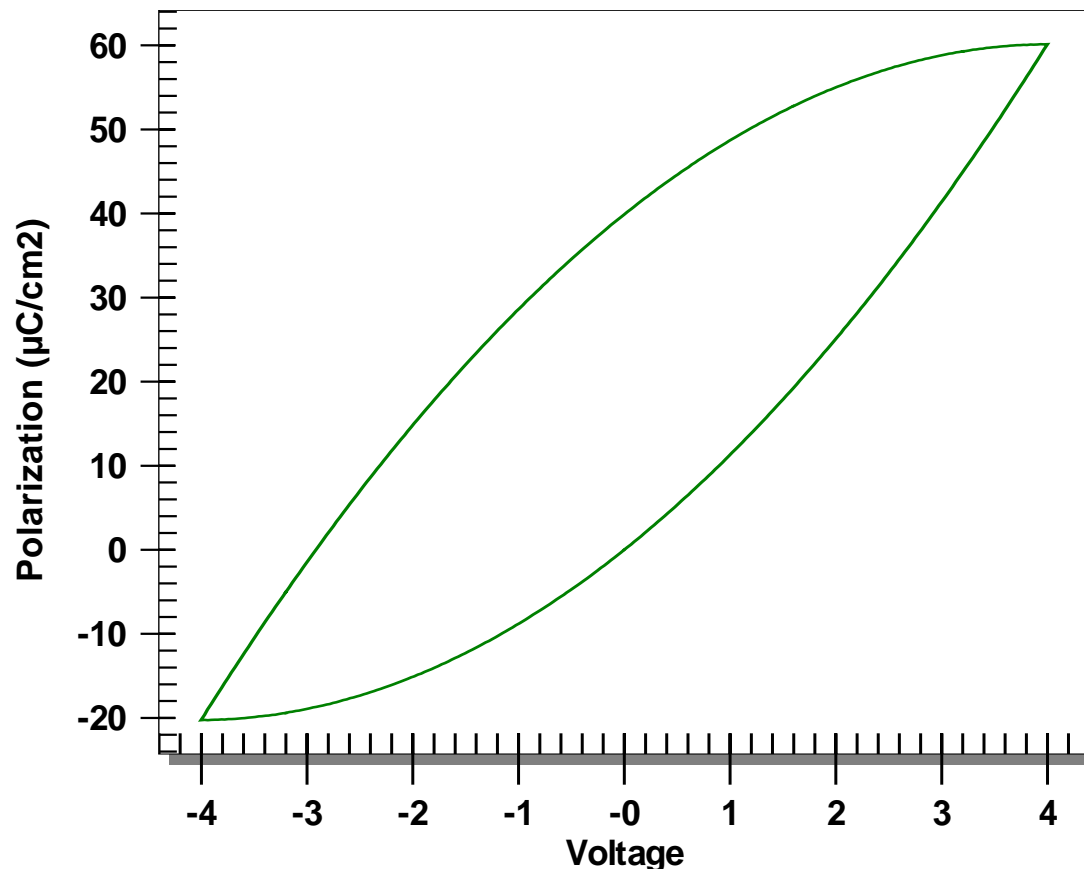


# What is this?



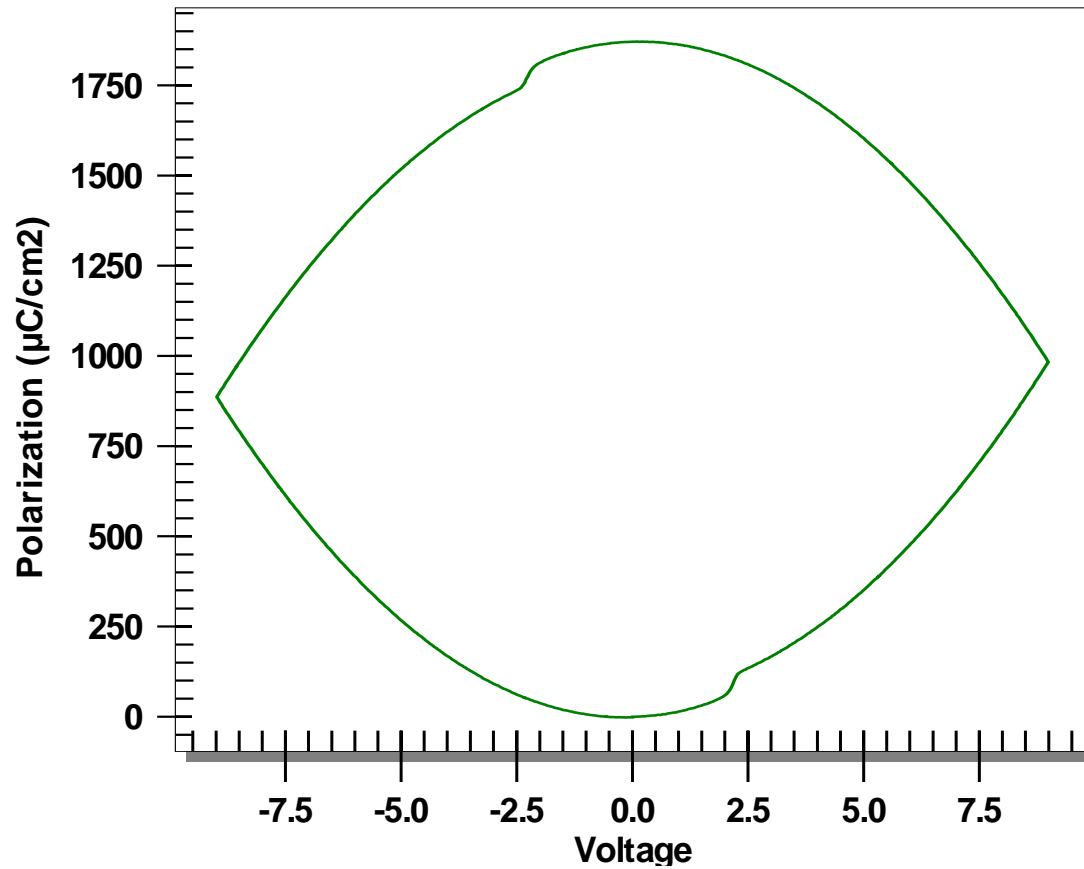
- Real clean. This one is easy.

# A Harder One

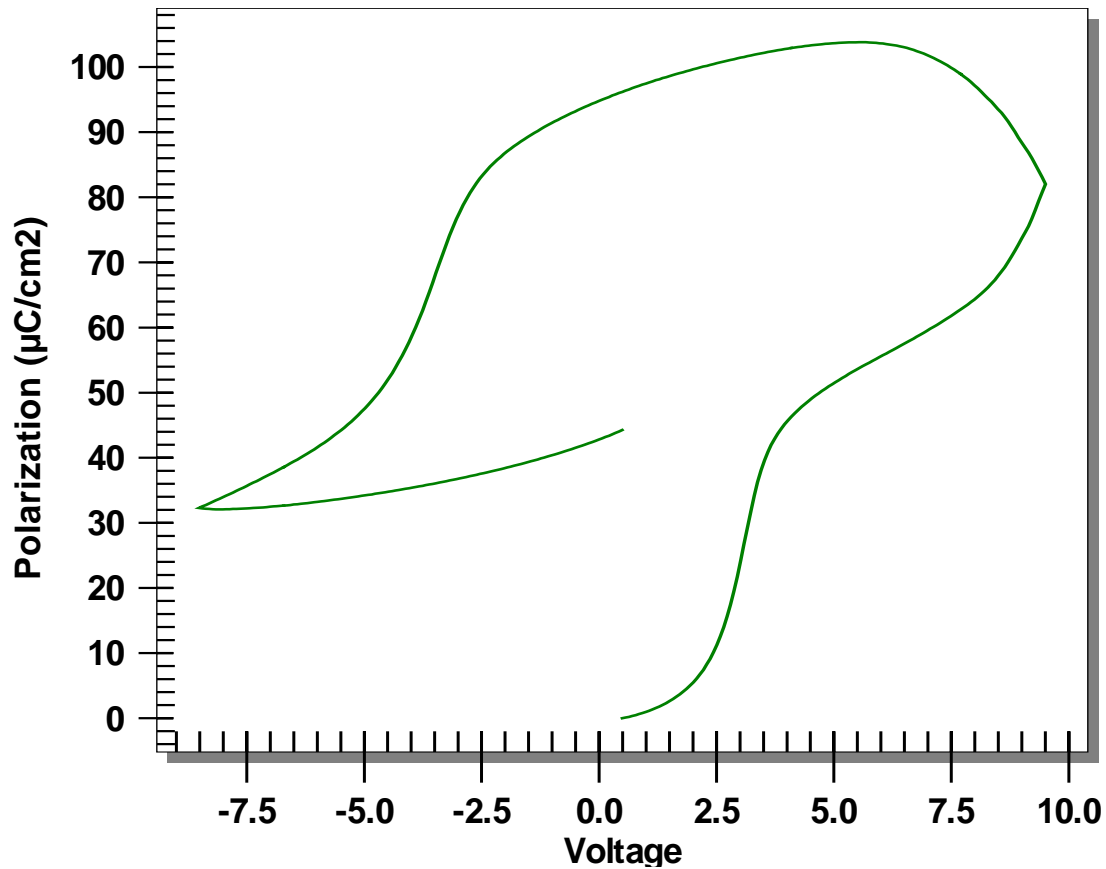


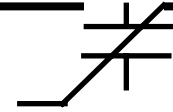
- Quite a few papers include loops that look like this.

# Is this Ferroelectric?



# What Happened Here?

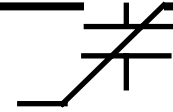




# Modeling Nonlinear Capacitance

- In electrical engineering, a fundamental approach to understanding a system is to break it into components and model each component.
  - Each component responds independently to the stimulus.
  - The output of a component is either the input to another component or is summed with the outputs of other components to form the response of the device.





# The Components

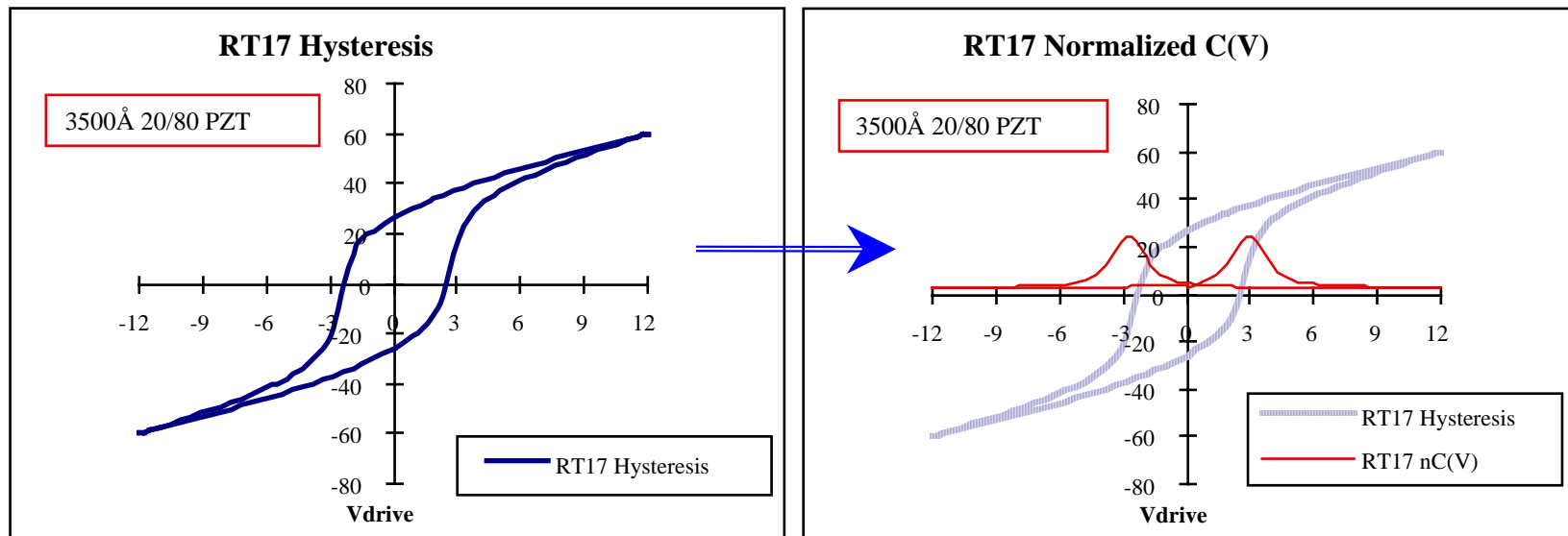
- According to Joe:
  - Linear capacitance
  - Non-linear capacitance
  - Remanent polarization
  - Remanent and nonremanent leakage
  - Remanent and nonremanent small signal capacitance
  - Reverse bias diode electrode interfaces
  - Left-overs

# A Mathematical Tool

The hysteresis loop is polarization responding to applied voltage:  $P(V)$ . Its derivative with respect to voltage is

$$\delta P / \delta V \Rightarrow (\delta Q / \delta V) / \text{Area}$$

which equals Large Signal Capacitance per Unit Area.



# Normalized CV

The normalized CV [**nCV**] has the formula

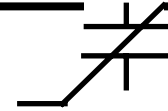
$$\delta P / \delta V \Rightarrow (\delta Q / \delta V) / \text{Area}$$

and has the units of

$$\mu\text{F}/\text{cm}^2$$

when the derivation is performed on the polarization units of

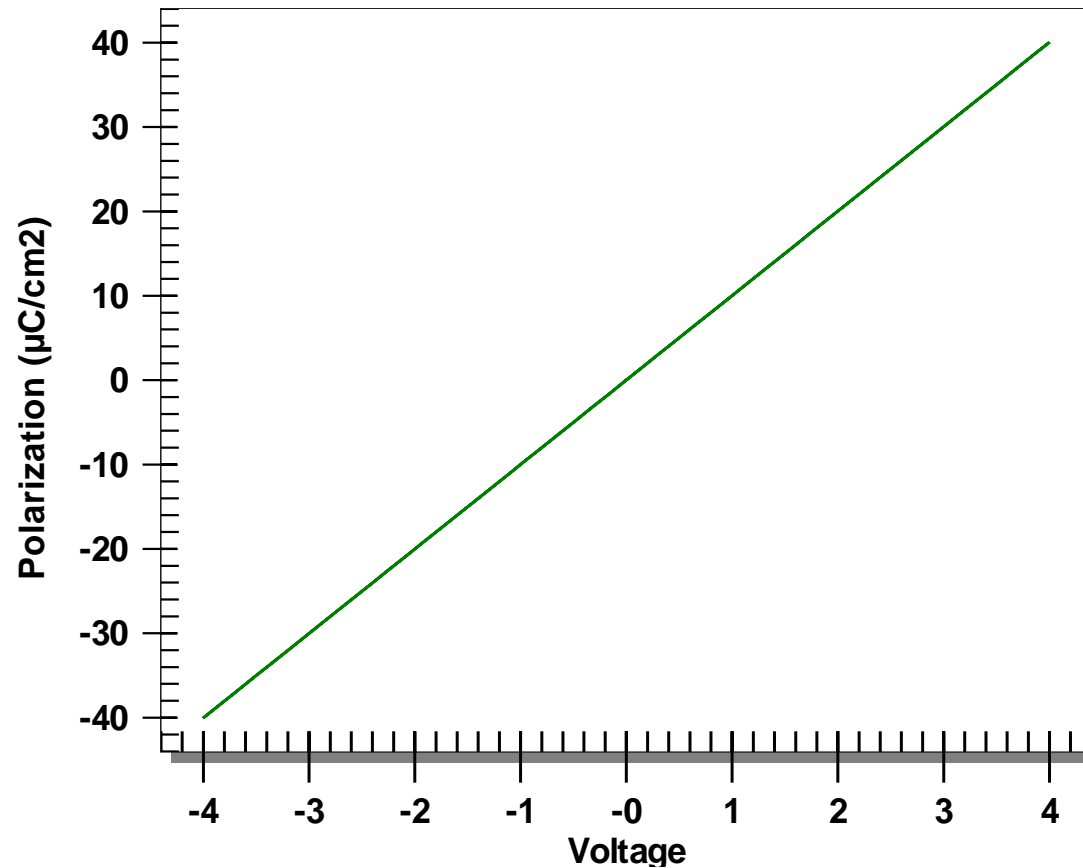
$$\mu\text{C}/\text{cm}^2.$$



# Integration

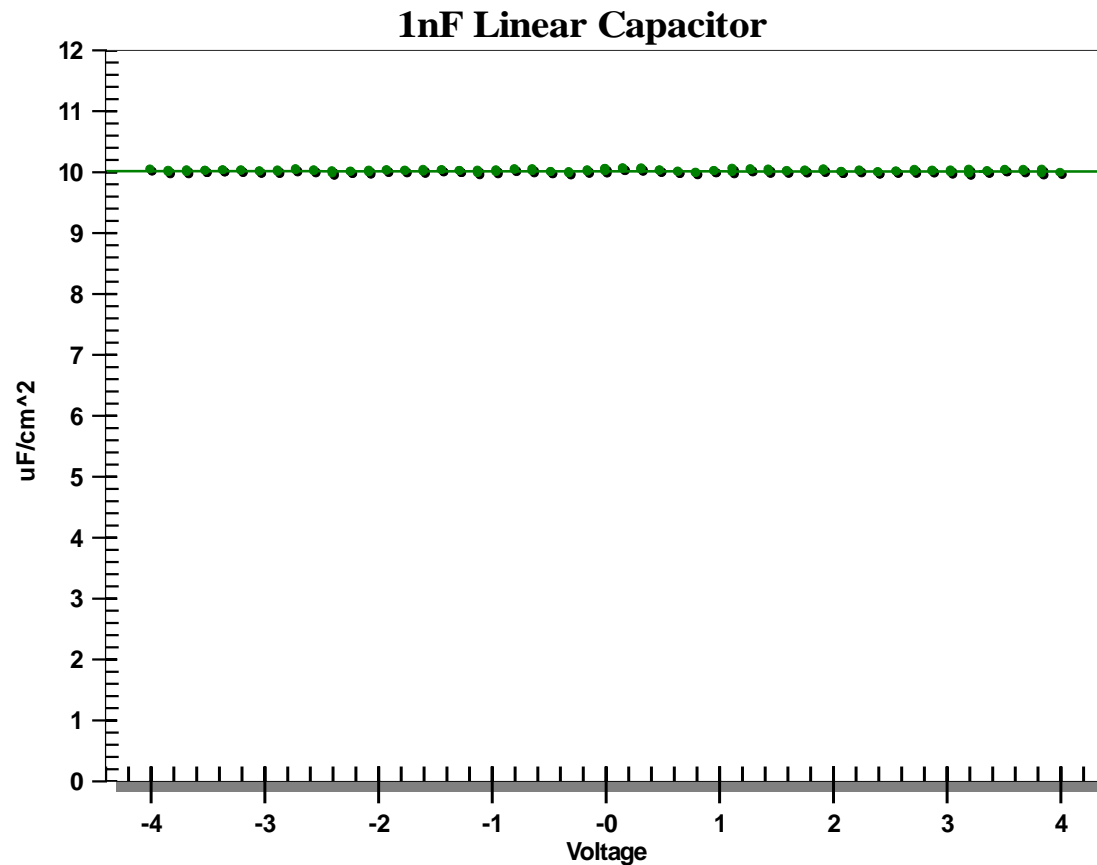
- Some measurements determine capacitance.
  - Small signal capacitance vs. Voltage
- Mathematical integration will convert the capacitance to its equivalent polarization contribution at each voltage.

# Linear Capacitance

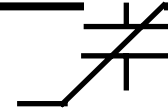


- $Q = C \times V$  where  $C$  is a constant

# Derivative of Linear Capacitance

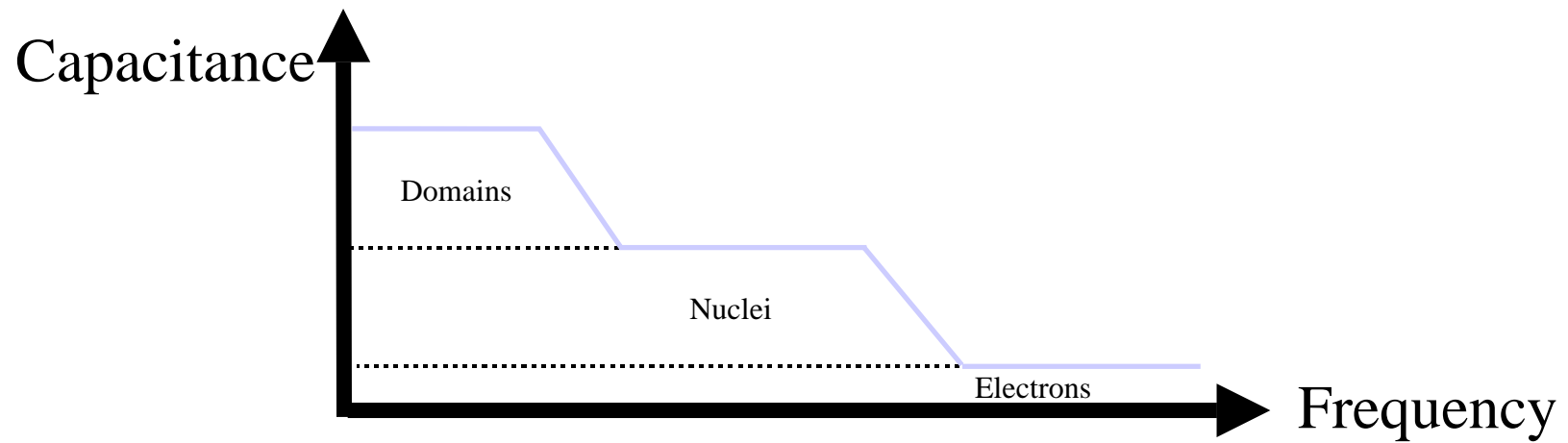


- C is a constant slope so the derivative of linear capacitance is simply a vertical offset on the nCV plot.



# Capacitance vs Frequency

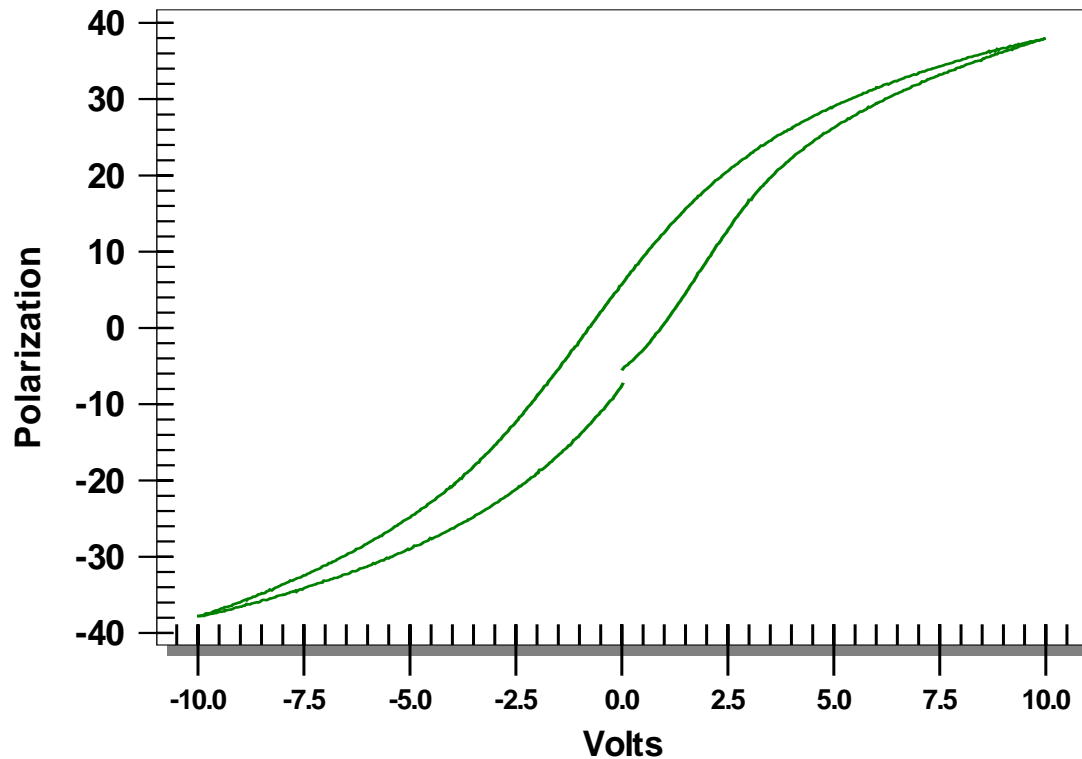
- Capacitance is about *separation* of charge!
  - Electrons are fast (light speed!).
  - Atoms are slow!
  - Domains are *real* slow!



# Non-linear Capacitance

Radiant 9/65/35 PLZT

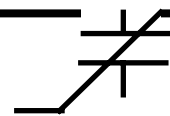
[ 1700Å ]



- When the electric field begins to move atoms in the lattice, the lattice stretches, changing its spring constant. Capacitance goes down.

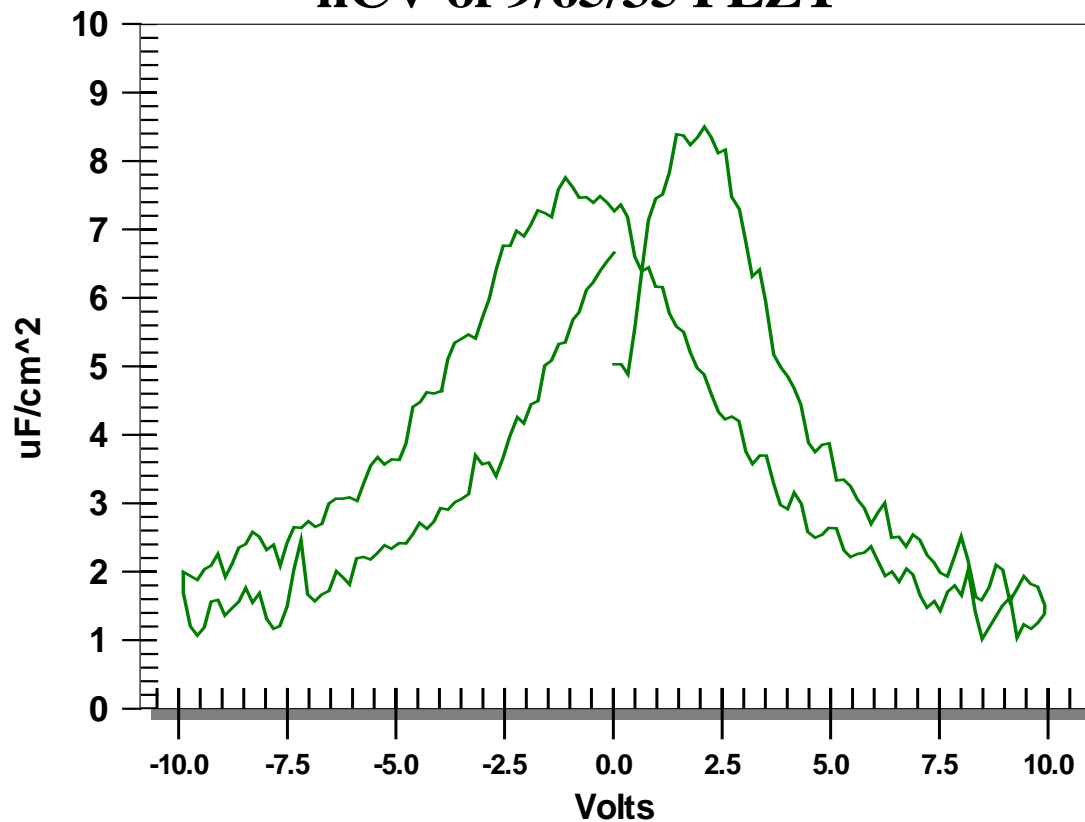
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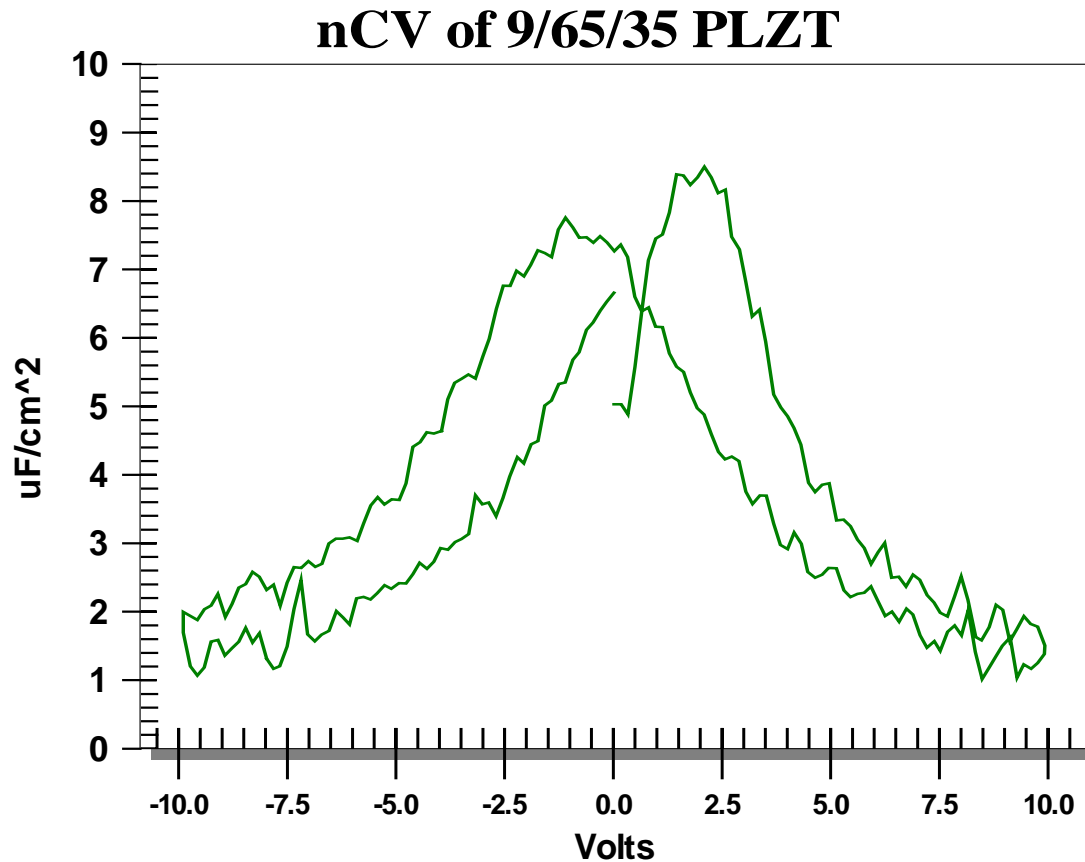
# The Derivative

nCV of 9/65/35 PLZT



A non-linear capacitor has decreasing capacitance as the applied voltage increases.

# Linear vs. Non-linear Capacitance

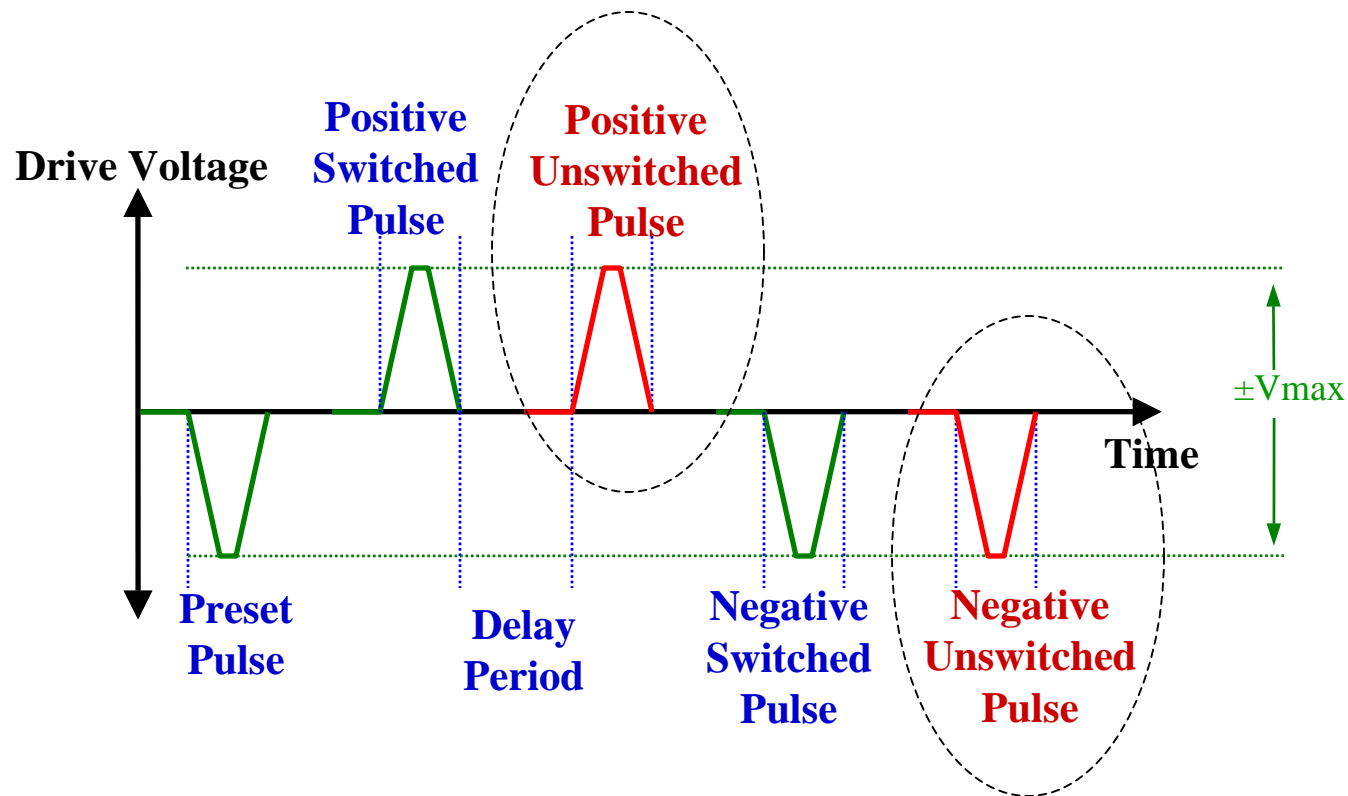


This device has both linear and non-linear capacitance. The linear capacitance is the vertical offset of the nCV plot. The tips do not touch zero.

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# Remanent Polarization

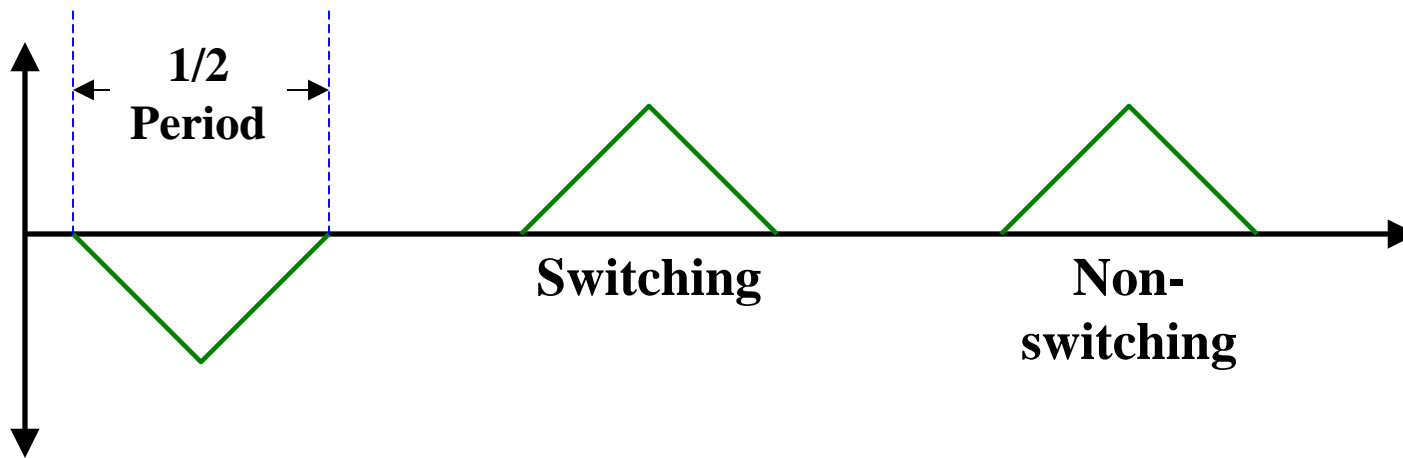
- The PUND test is a familiar measurement:



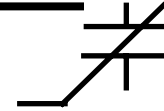
- Any matched pair of switched and non-switched pulses may be subtracted from each other to get the remanent polarization.

# Remanent Hysteresis

- The same measurement may be made using half-hysteresis loops instead of pulses:

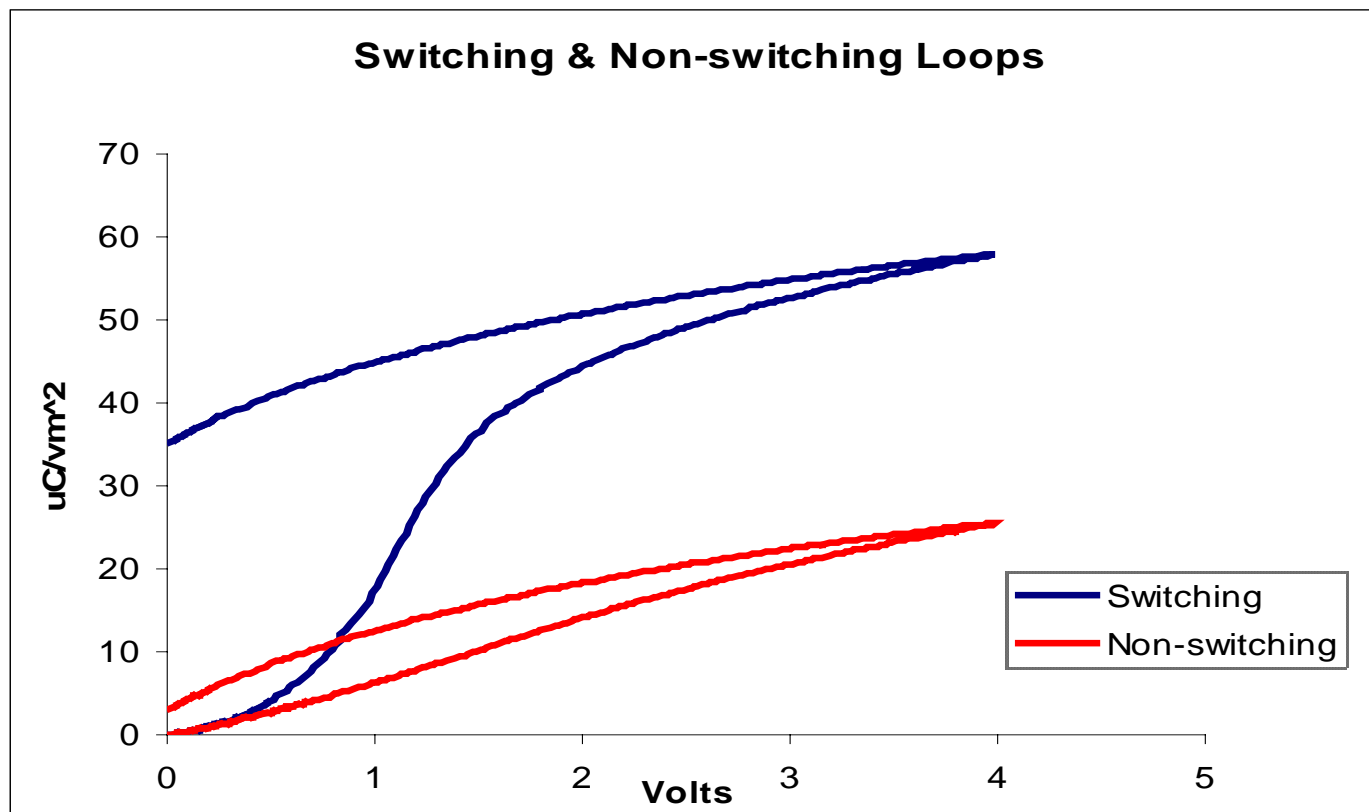


- The difference between the switching and non-switching measurements will give the Remanent Polarization vs Voltage function.



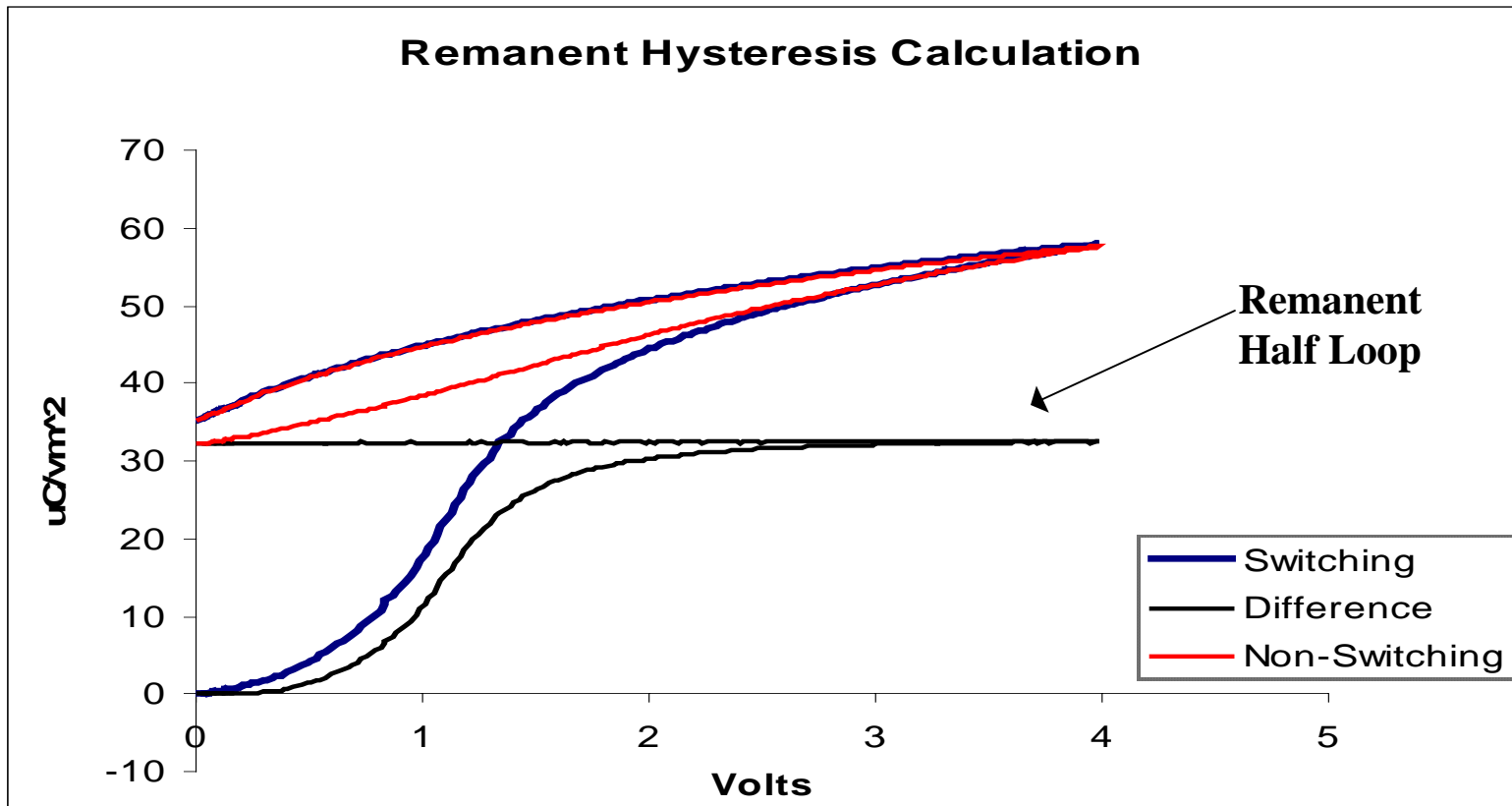
# Remanent Hysteresis

Switching and Non-switching half loops:



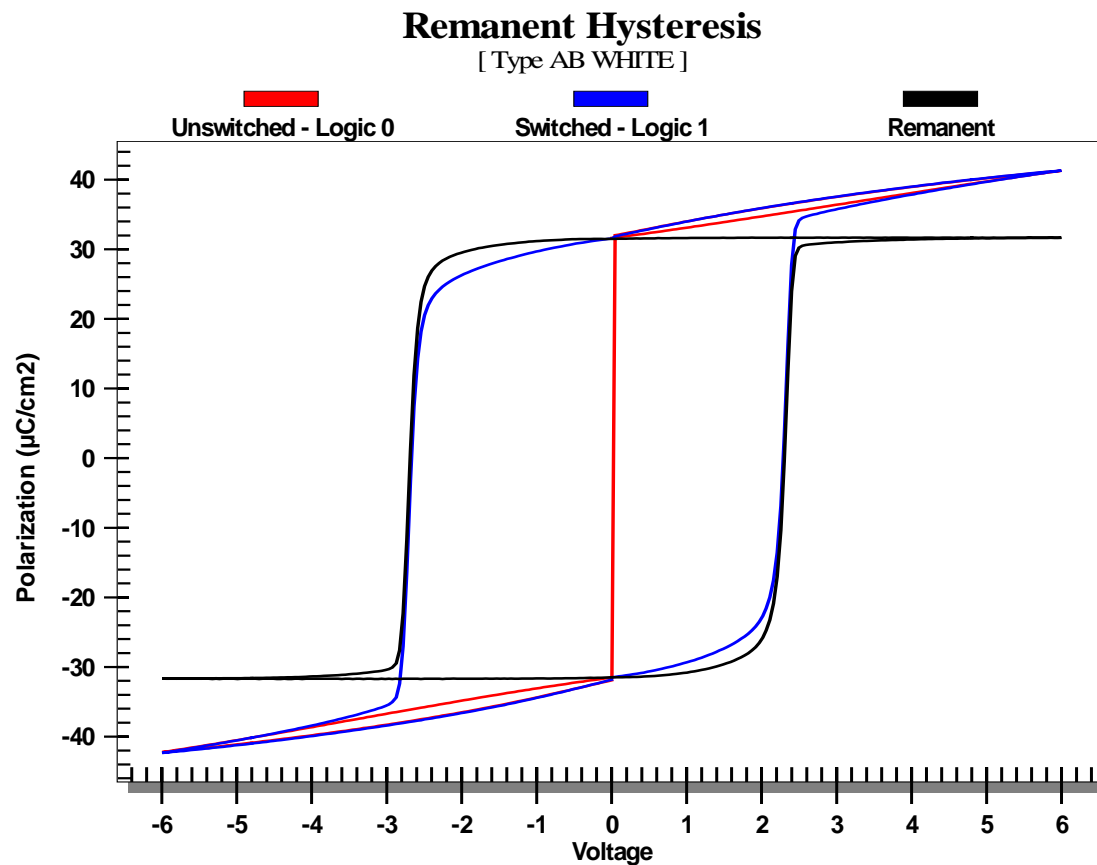
# Remanent Hysteresis

- PUND:  $P^*_r - P^r = dP = Q_{switched}$
- Hysteresis: Switching - Non-switching = Remanence:



# Remanent Hysteresis

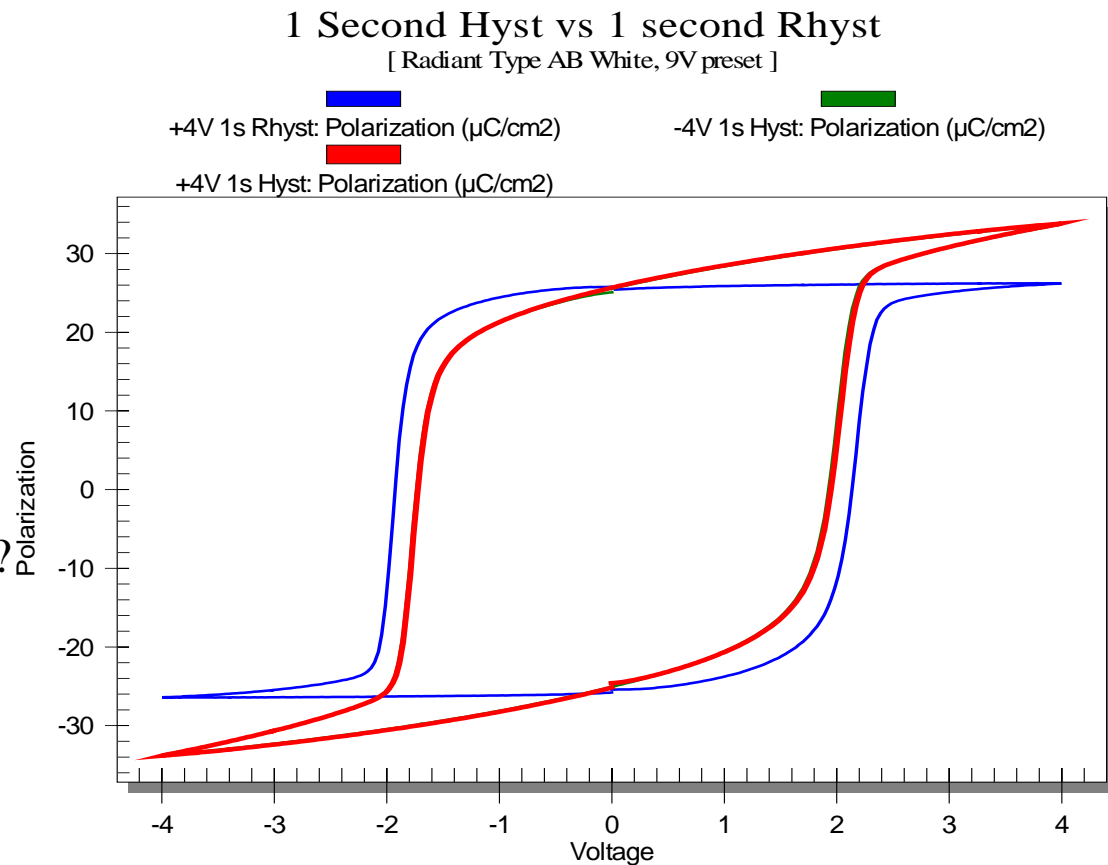
- The test may be executed in both voltage directions and the two halves joined to show the switching of the remanent polarization that takes place *inside* the full loop.



# Remanent vs. Normal Hysteresis

- The first stage of the experiment consisted of measuring two 4V hysteresis loops going in opposite directions (including their gaps) and a 4V remanent polarization loop.

- The remanent hysteresis is in blue.
- The **full loops** in opposite directions overlay exactly.
- The  $V_c$  of the remanent loop lies outside that of the normal loops. Why? (Hint: the reason is purely mathematical.)
- The  $V_c$  of the remanent loop is the true  $V_c$ .

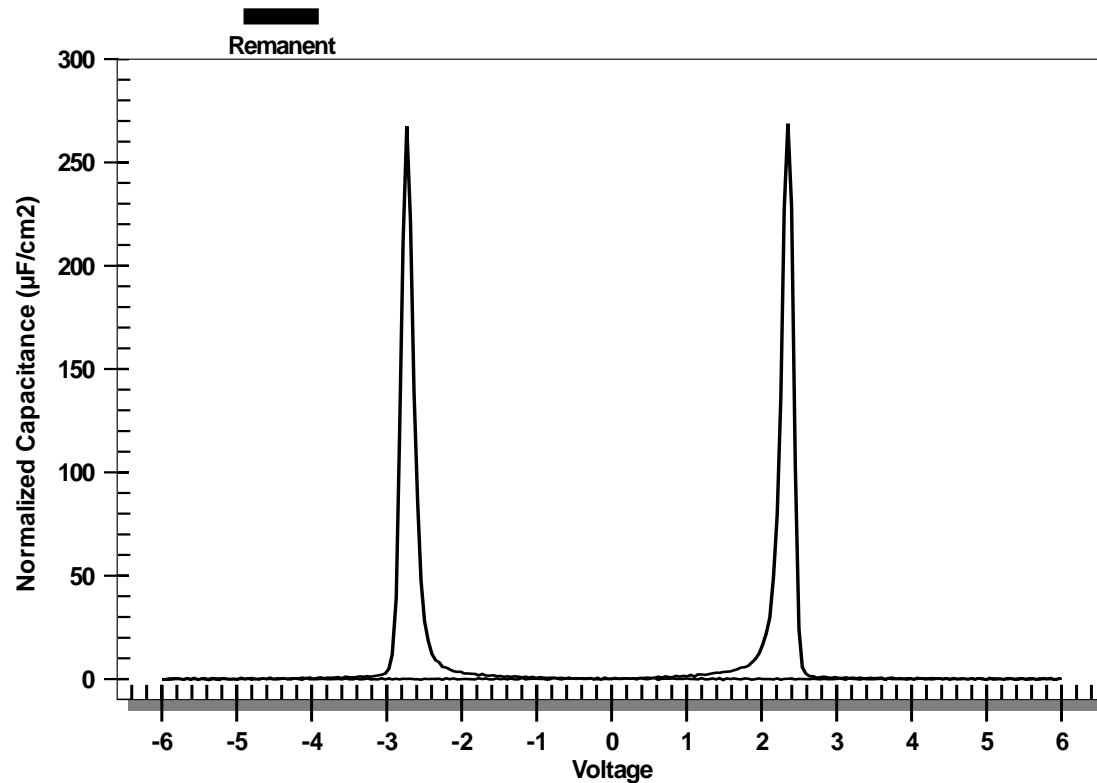




# The Derivative

## nCV of Remanent Hysteresis Loop

[ Type AB ]

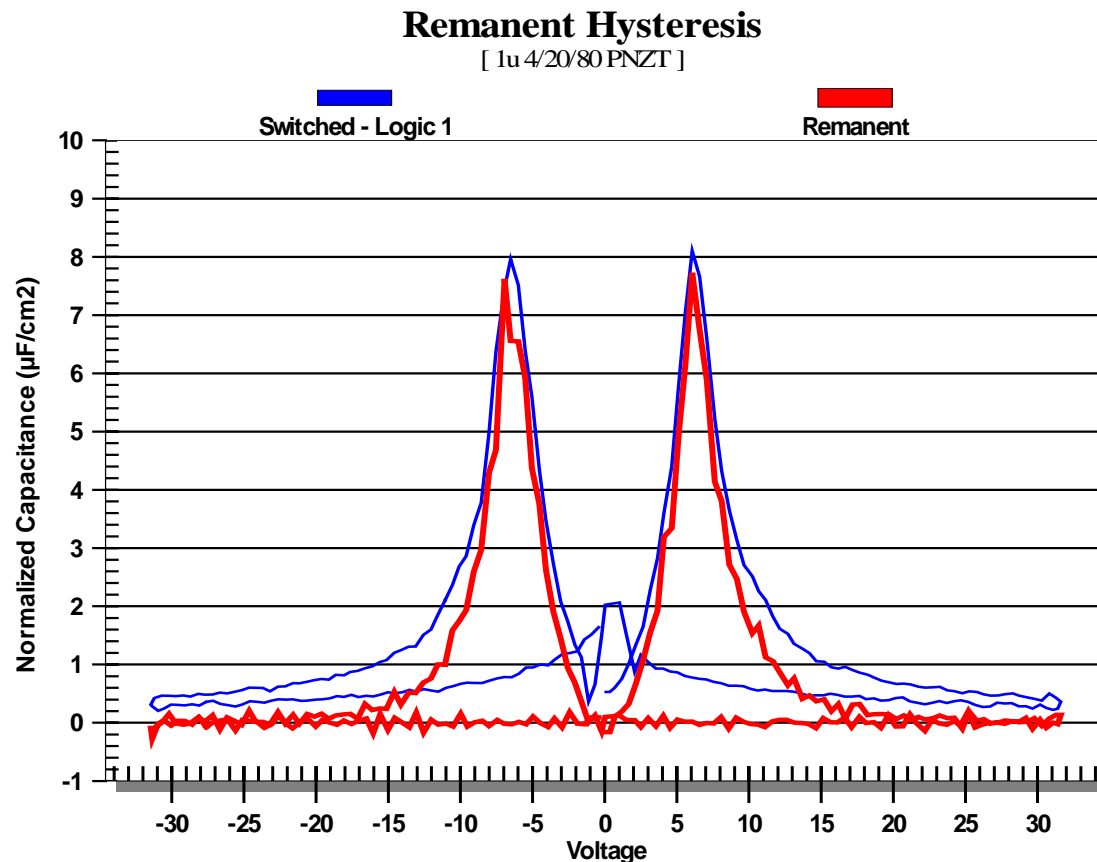


- The nCV of the remanent polarization loop rests on the X-axis because it has no capacitance on the re-trace.

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# The Perfect Capacitor

- A perfect capacitor combines non-linear capacitance with remanent polarization.



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# Hysteresis in Small Signal Capacitance

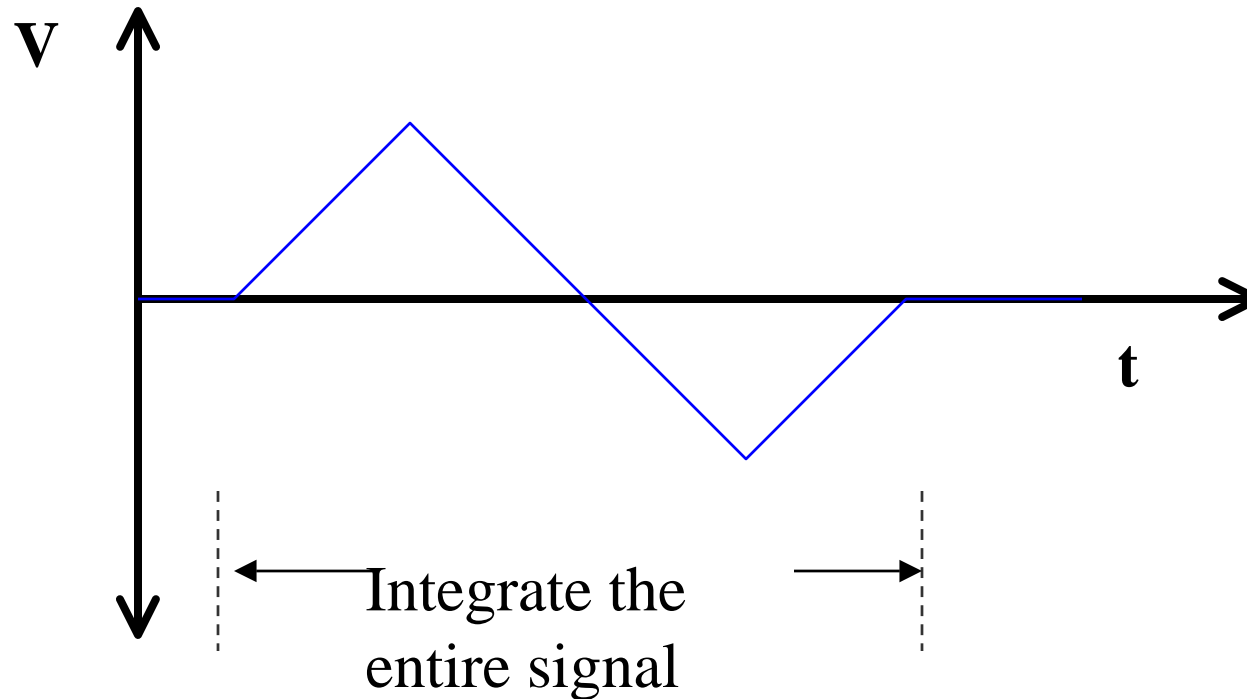
- The small signal capacitance versus bias voltage is determined by measuring the sample capacitance with a low amplitude signal at a series of bias voltages.
  - Theoretically, the signal amplitude should be small enough that it does not disturb the state of the capacitor.
- While this is a noble effort, it cannot be ignored that the remanent polarization modulates the small signal capacitance.
- The state of the remanent polarization must be managed during measurements of small signal capacitance.



# Small Signal vs Large Signal

- The ferroelectric hysteresis measurement is defined at Radiant as a “large signal” measurement of the polarization properties of the sample.
- “Large signal” means that the test waveform has a large enough amplitude to switch dipoles in the ferroelectric material.
- As well, the “large signal” measurement captures and integrates all changes the sample experiences during the test waveform, showing its entire trajectory.
- The measurement result contains contributions from all components of the sample, including the remanent polarization and parasitics.

# Small Signal vs Large Signal



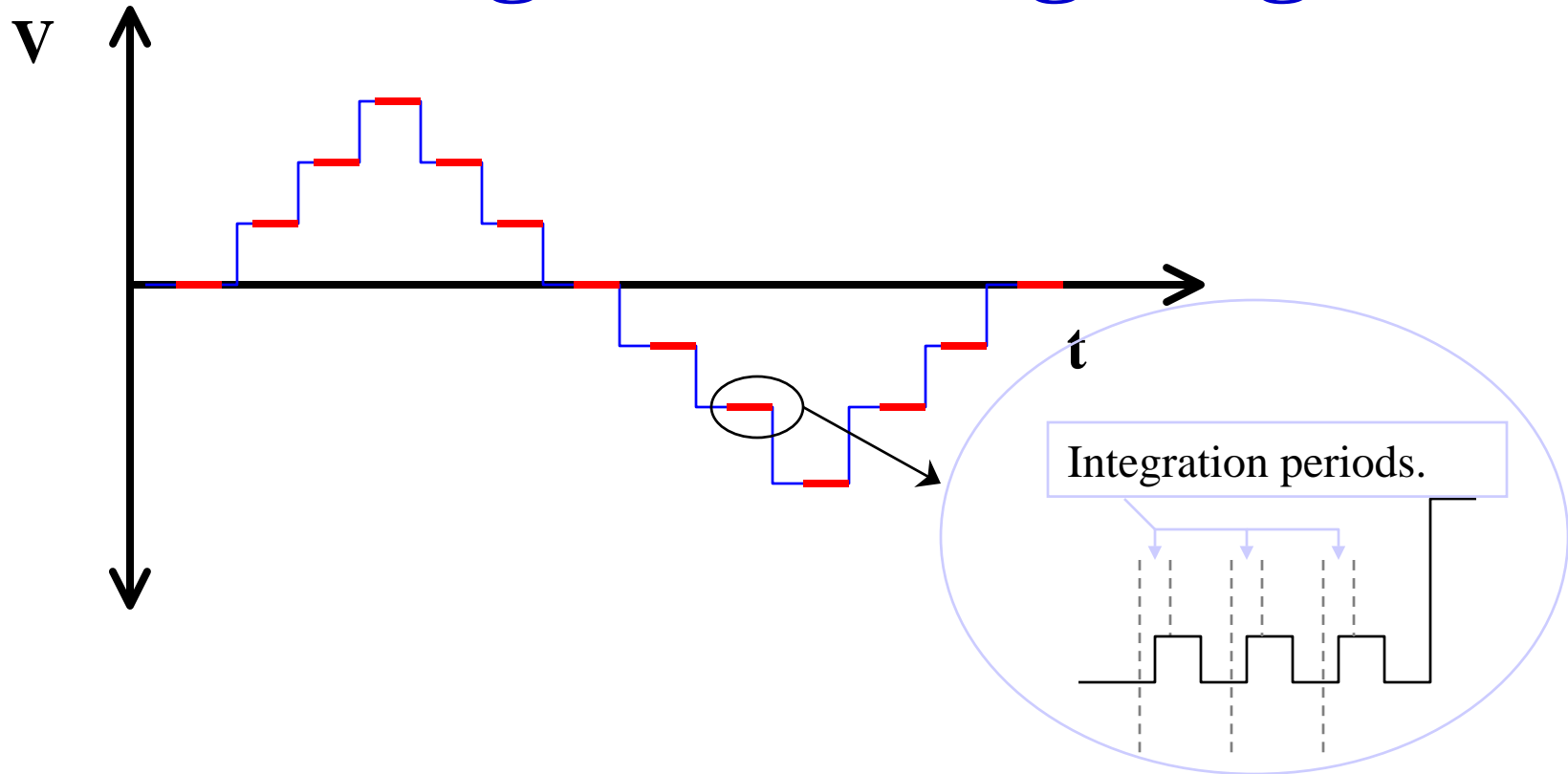
- A “large signal” measurement captures every electron that moves into or out of the capacitor during the stimulus waveform.

# Small Signal vs Large Signal

- The “small signal” measurement is defined as one where the test amplitude is small compared to that required to switch remanent polarization in a ferroelectric capacitor.
- Since the response of a non-linear sample changes with the absolute value of the voltage applied and the remanent polarization state, the “small signal” measurement must also have a steady state voltage component as well as a remanent polarization pre-set procedure to put the sample in the appropriate state.
- Therefore, the “small signal” measurement captures and integrates only those changes the sample experiences during a small amplitude stimulation of the sample at a specified voltage and polarization state.

By definition, the “small signal” measurement contains no contribution from switching dipoles!

# Small Signal vs Large Signal



- In “small signal” measurements, many small measurements are taken that capture only the small changes associated with small stimuli.
- In a “small signal” measurement, the sequence of DC bias values is the same as the voltage profile used for hysteresis so the two can be compared directly.



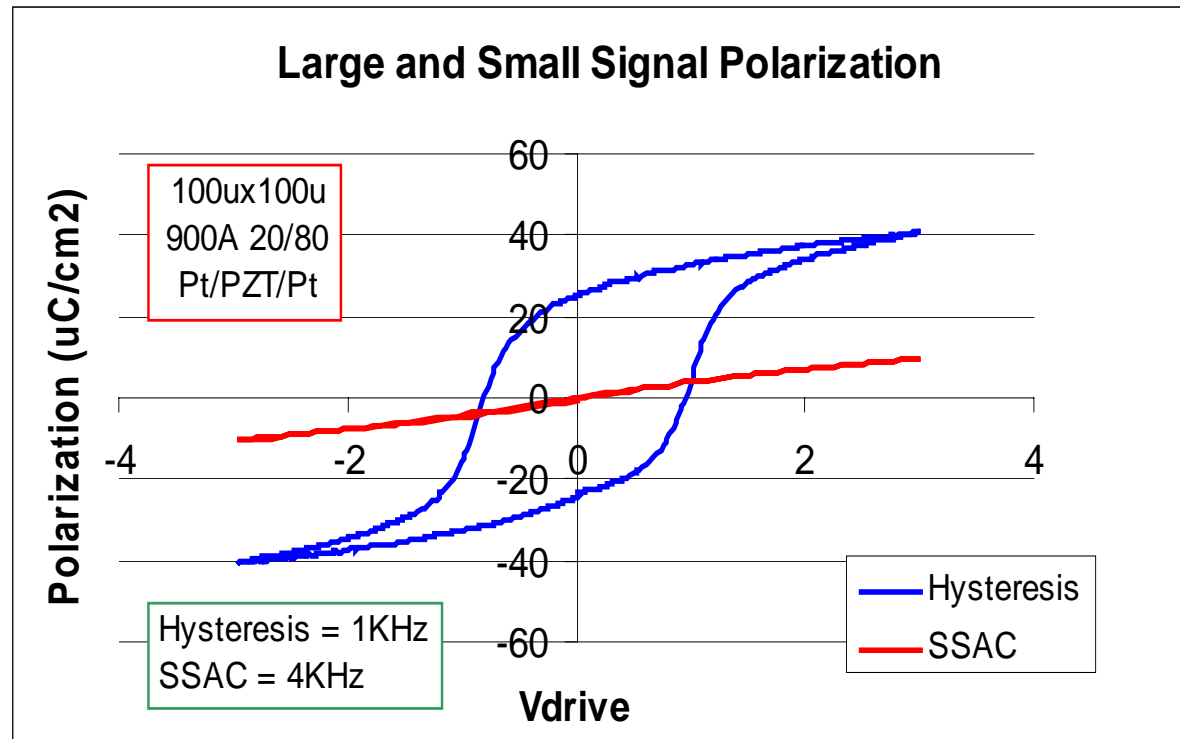
# Small Signal vs Large Signal

- Radiant testers execute both standard “large signal” hysteresis and “small signal” capacitance measurements.
  - “large signal” hysteresis results are normally given in units of polarization ( $\mu\text{C}/\text{cm}^2$ ) but can be converted to capacitance using the CV or Normalized CV plotting functions of the Hysteresis Task or the Hysteresis Filter.
  - “small signal” measurements are normally given in units of capacitance (nF or  $\mu\text{F}/\text{cm}^2$ ) but can be converted to equivalent polarization using the appropriate plotting function of the Advanced CV measurement task.



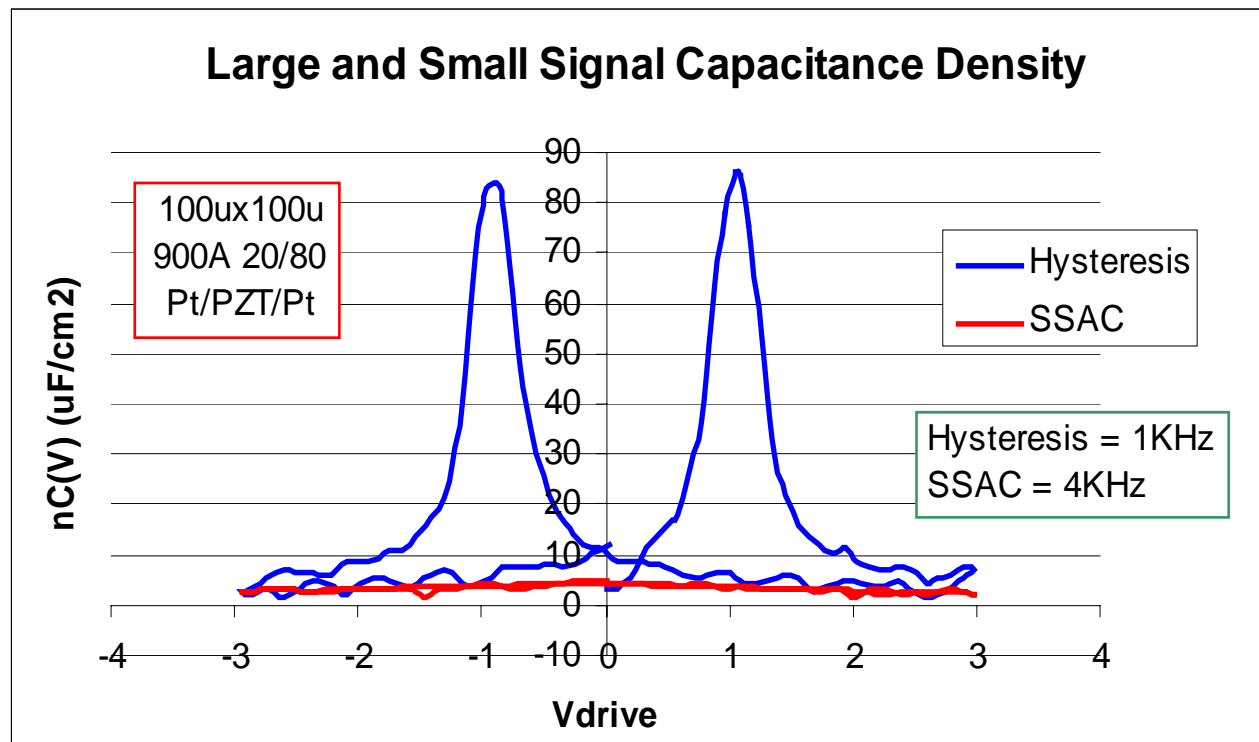
# Small Signal vs Large Signal

- Comparison of the Hysteresis and Polarization of the Small Signal Capacitance is shown below:

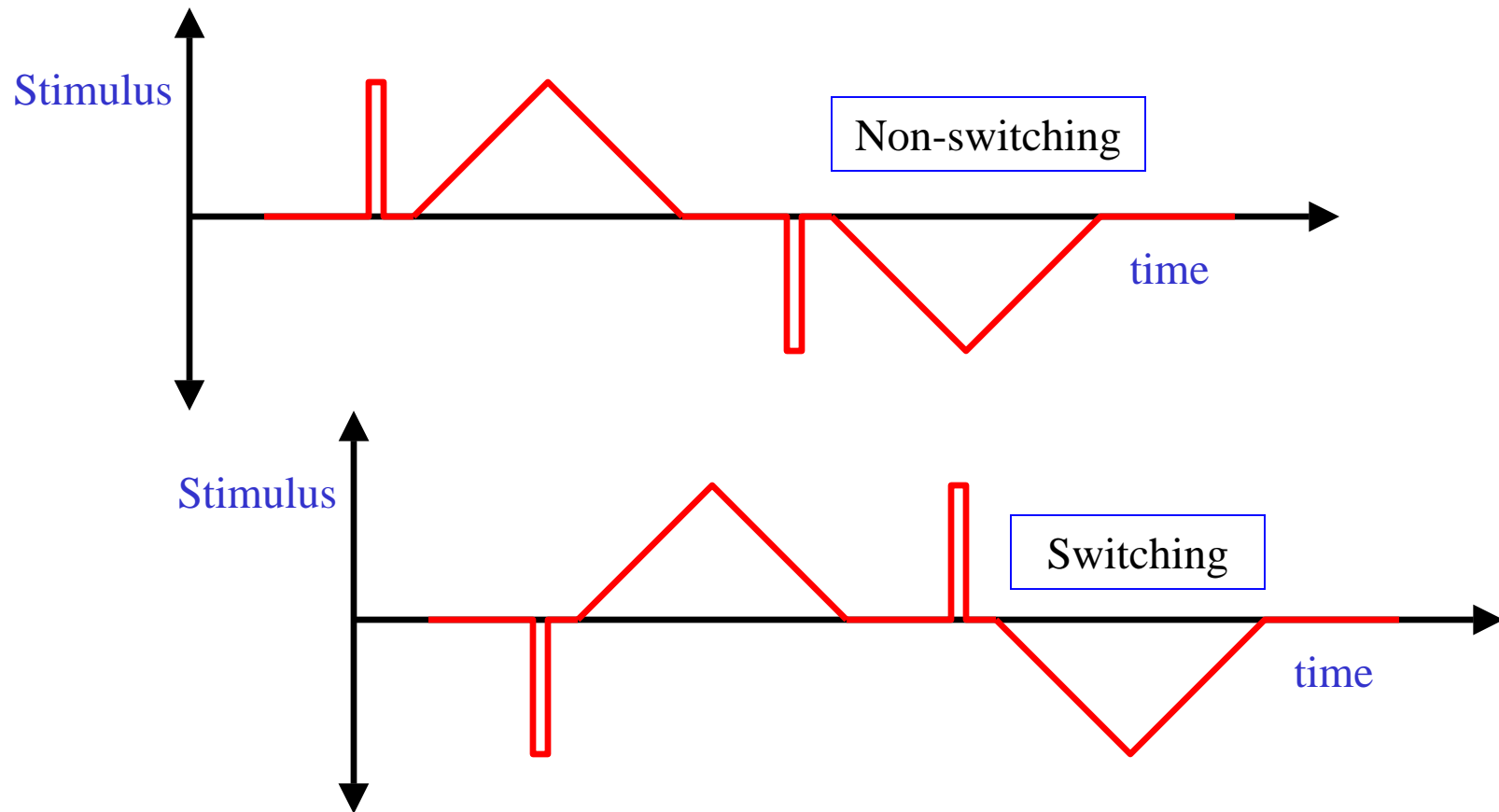


# Small Signal vs Large Signal

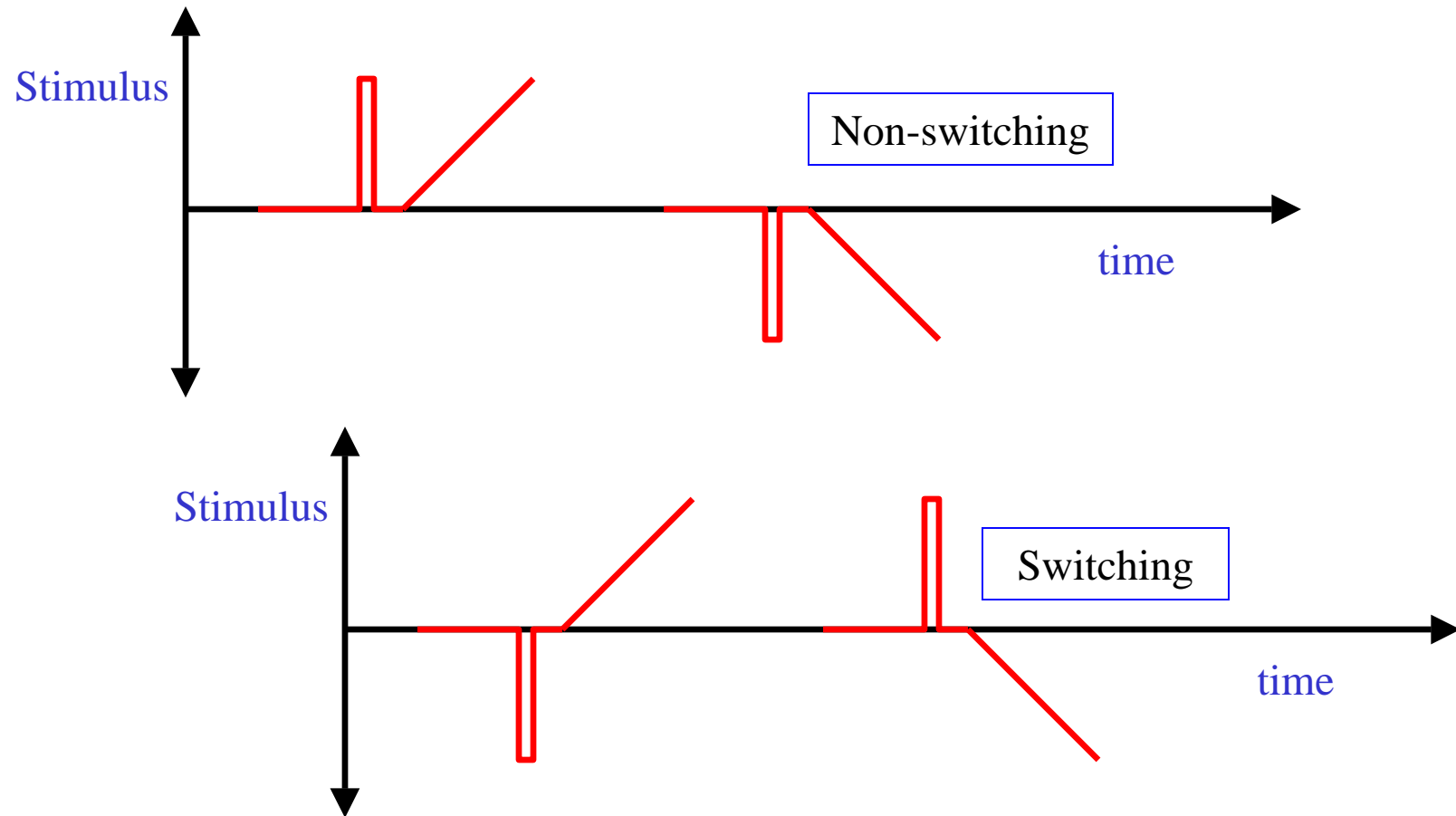
- Comparison of the Large and Small Signal Capacitance is shown below:

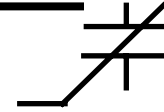


# Hysteresis in Small Signal Capacitance



# Hysteresis in Small Signal Capacitance

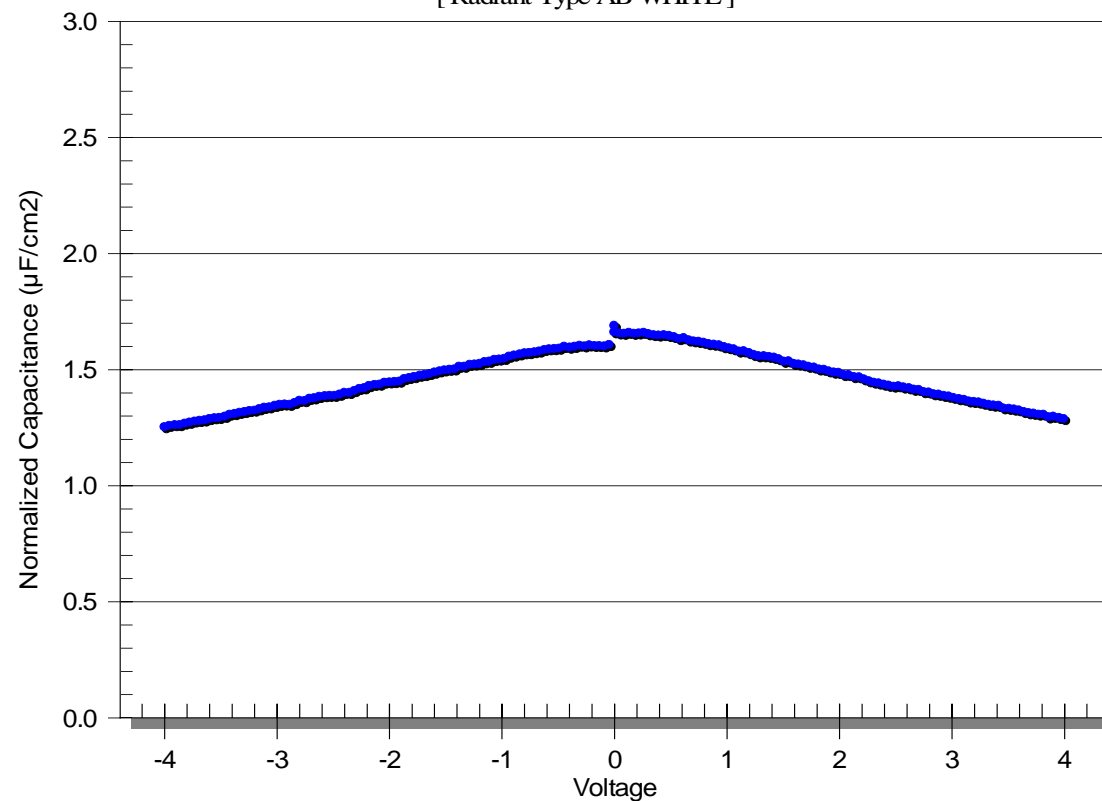




# Non-switching CV for the Sample under Test

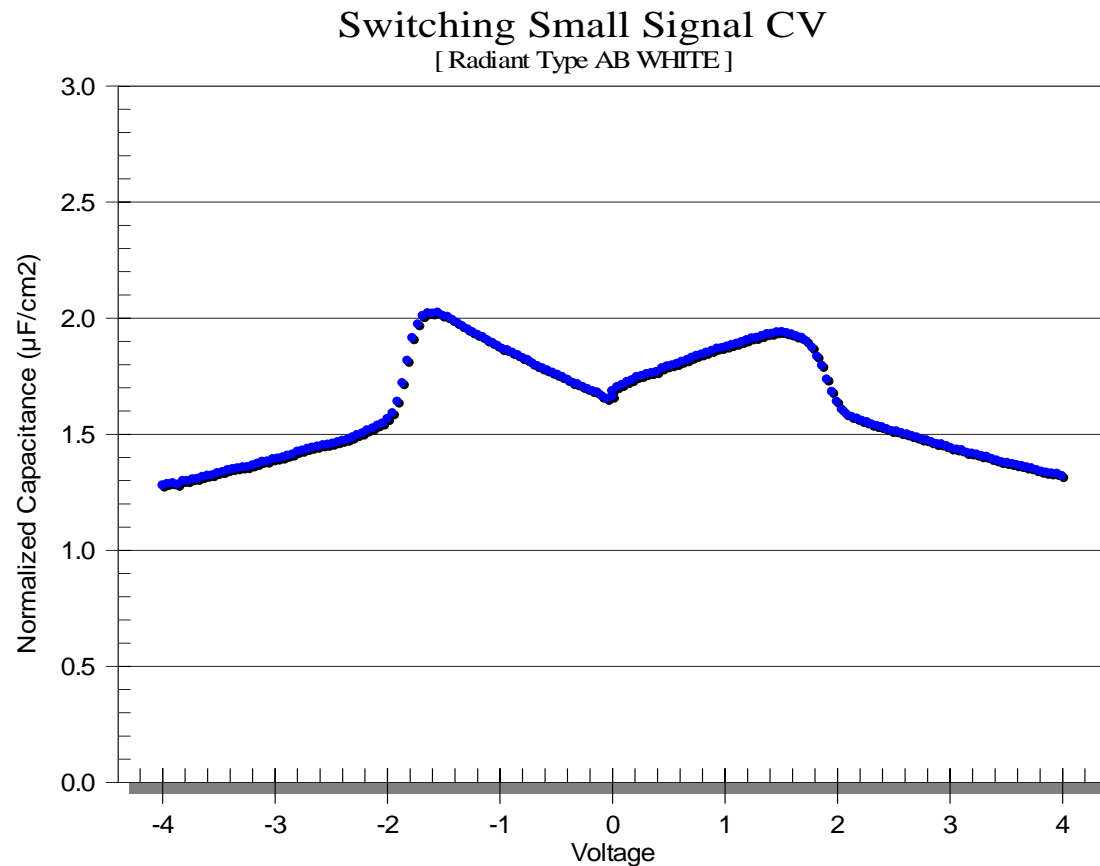
- 1KHz 0.2V test with 182 points

Non-switching Small Signal CV  
[ Radiant Type AB WHITE ]

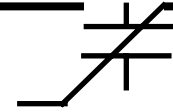


# Switching CV for the Sample under Test

- 1KHz 0.2V test with 182 points

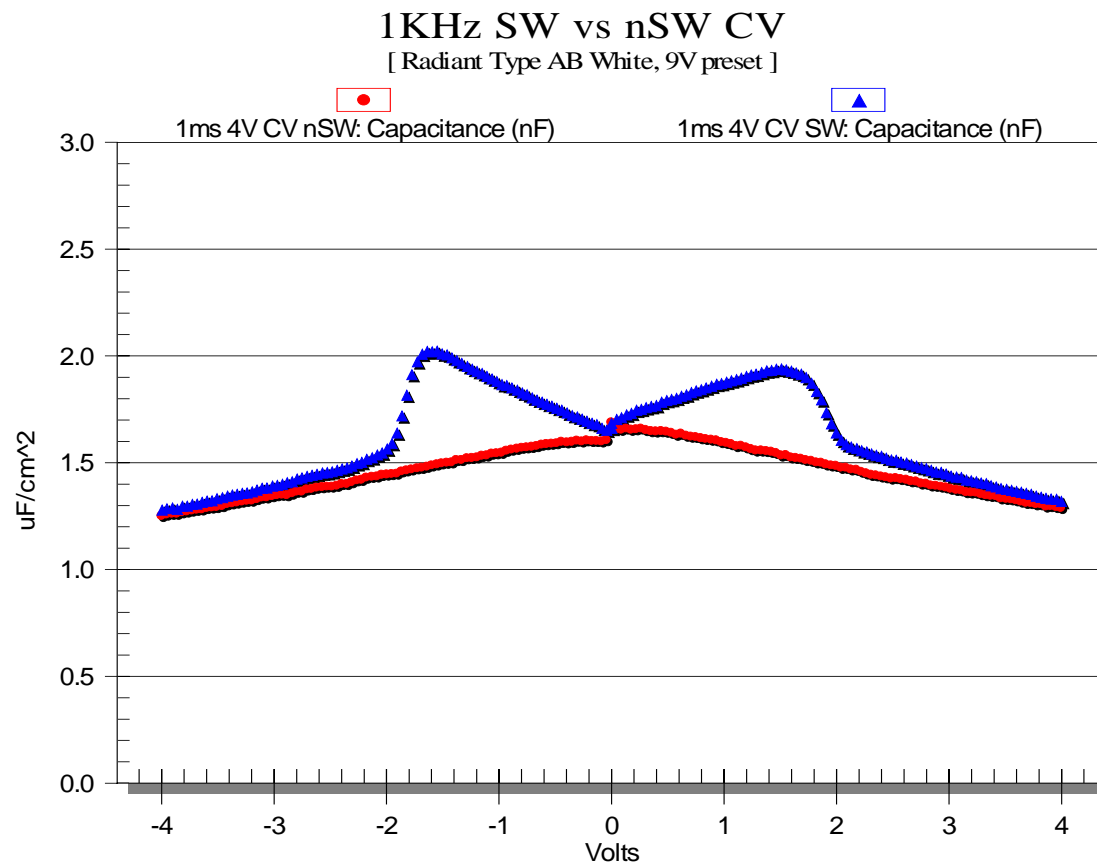


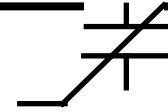
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# Non-switching vs Switching CV

- 1KHz 0.2V test with 182 points



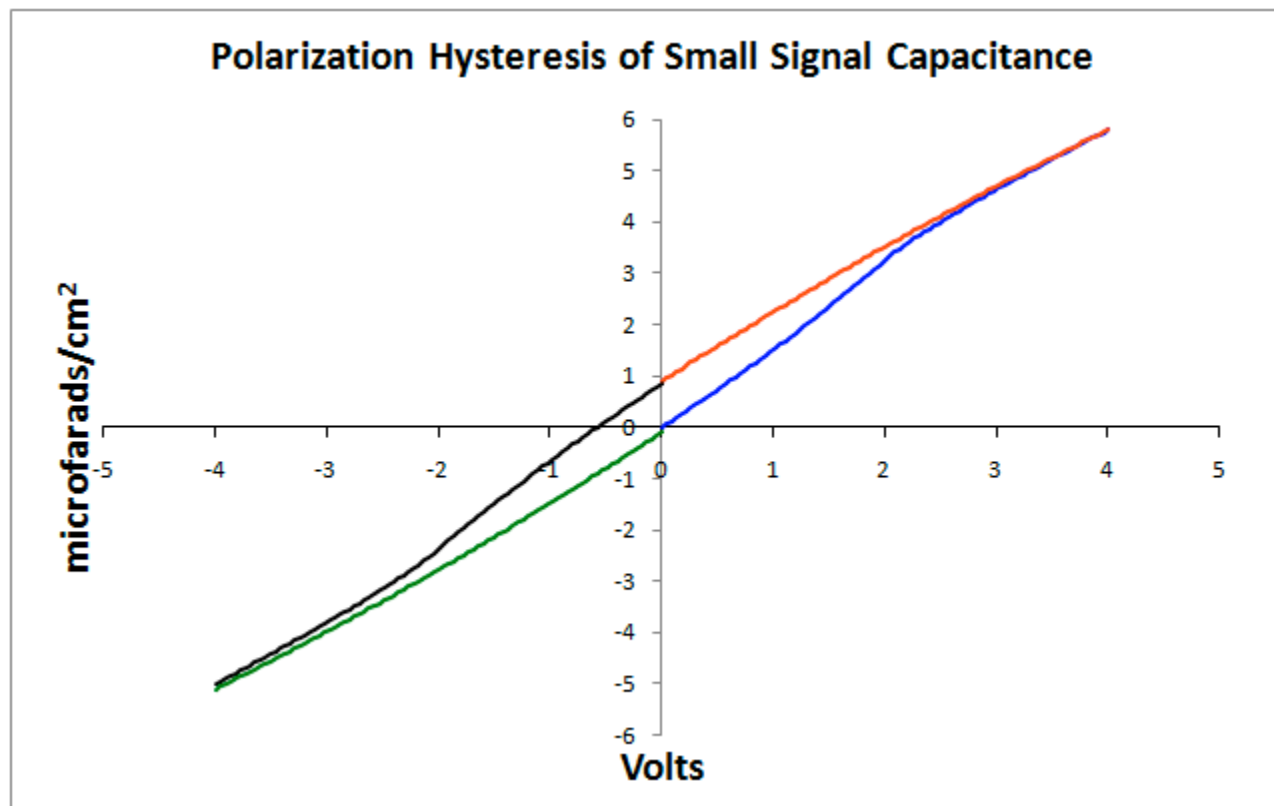


## Q vs V from Small Signal Capacitance

- The small signal capacitance can be multiplied by the  $dV$  to get the  $dQ$  per test step.
- The  $dQ$ s may be integrated to see the polarization hysteresis contributed by the modulation of small signal capacitance by remanent polarization!

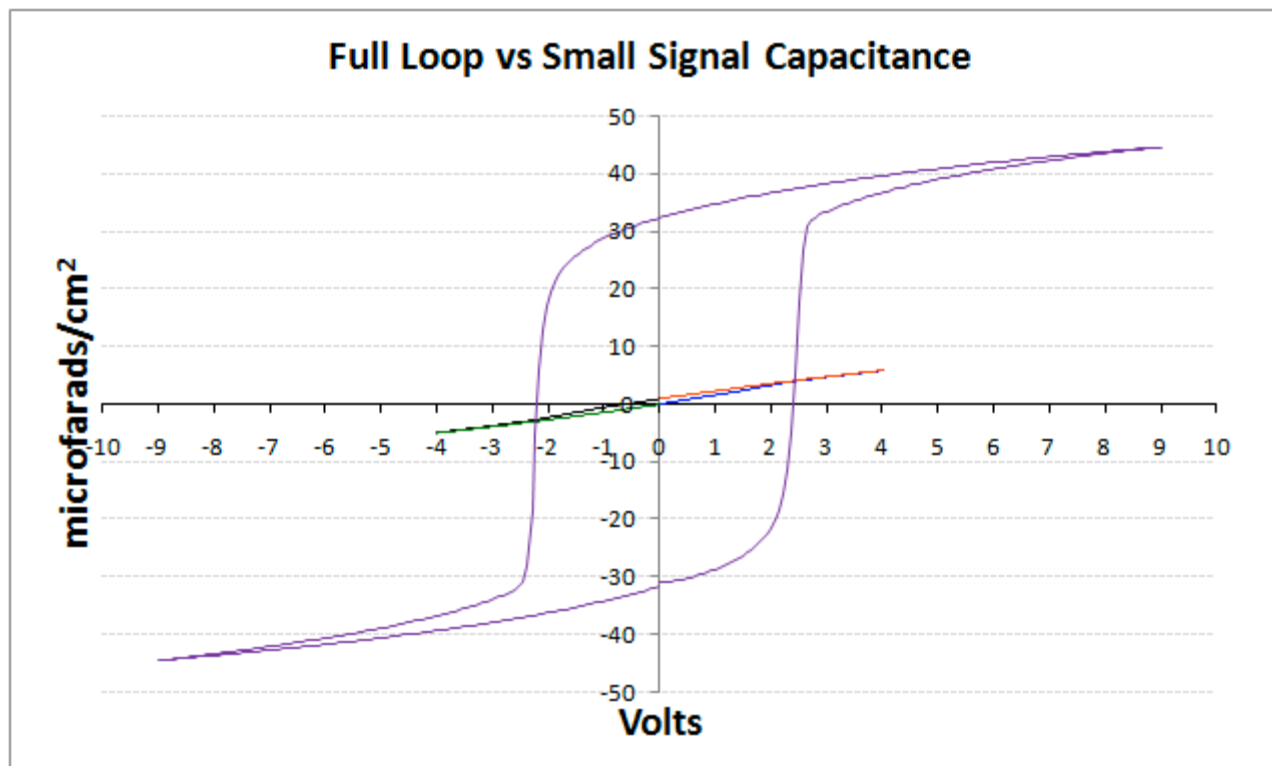


# Small Signal Capacitance Polarization



- Small signal capacitance forms a hysteresis of its own.

# Small Signal Capacitance Polarization

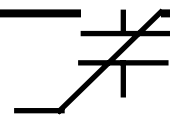


- The contribution of small signal capacitance hysteresis to the overall loop is small in this case.



# Resistive Leakage in a Hysteresis Loop

A common problem in ferroelectric ceramics is a linear resistance function. Usually, it appears due to leakage along grain boundaries although it can occur from dopants or defects in the grains themselves.

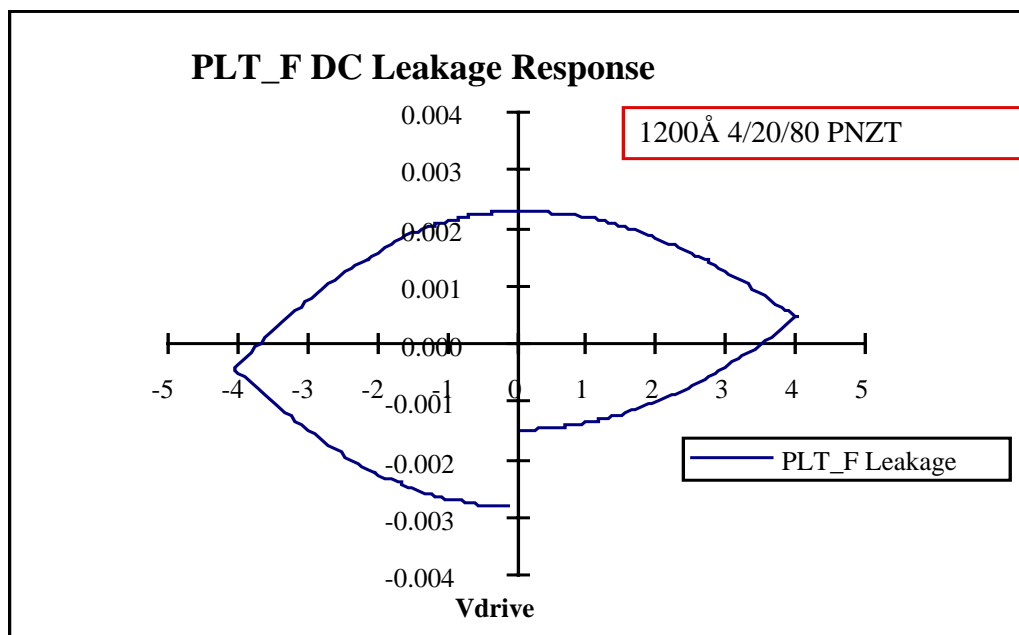


# Resistive Leakage in a Hysteresis Loop

*Linear* resistance is easy for a triangle wave:

$$\Delta P = (\text{Current} \cdot \Delta \text{time}) / \text{Area}$$

$$\therefore P = (\sum_{n=0}^k n \cdot \Delta V / R \cdot \Delta t) / \text{Area}$$

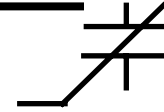


time=time step per point

V=fixed voltage step of

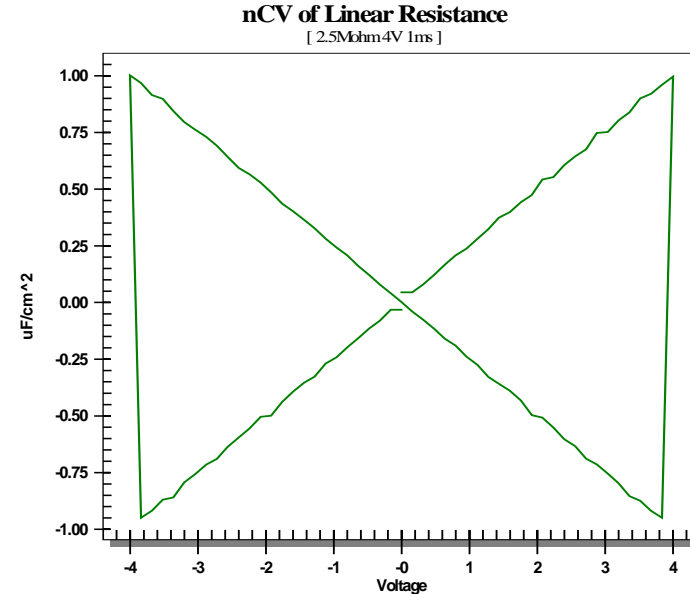
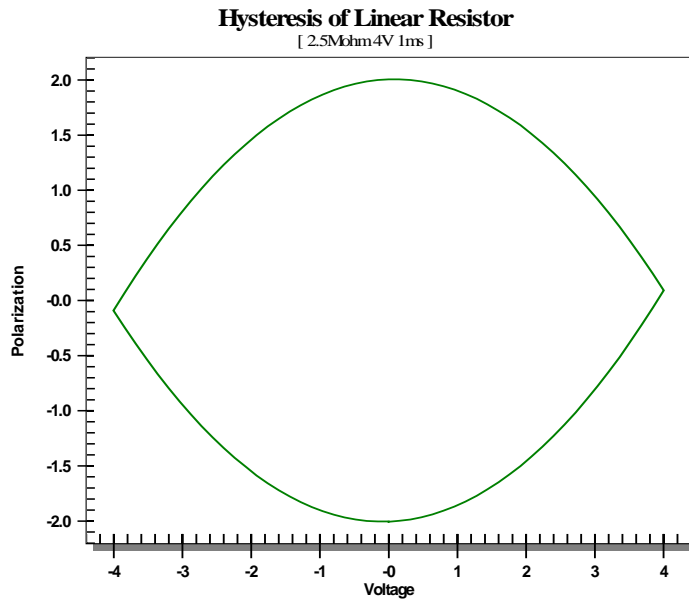
= point number of digitized triangle wave

result = "Football"

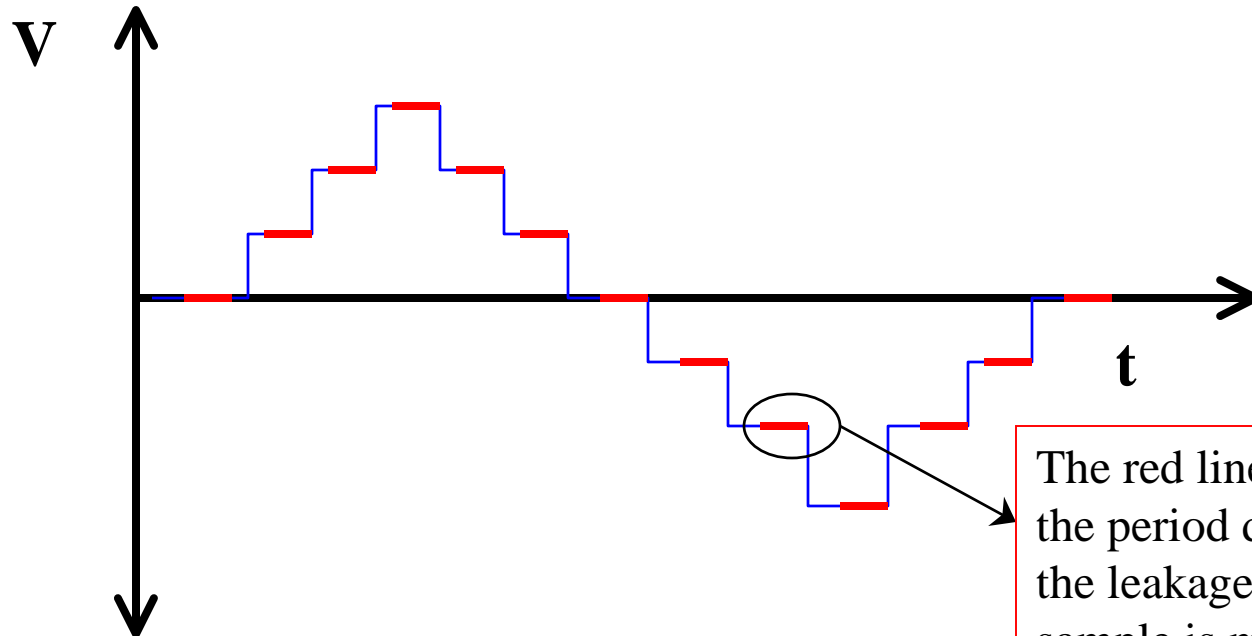


# Resistive Leakage in a Hysteresis Loop

The derivative of pure resistive leakage is an “X”.



# IV Test

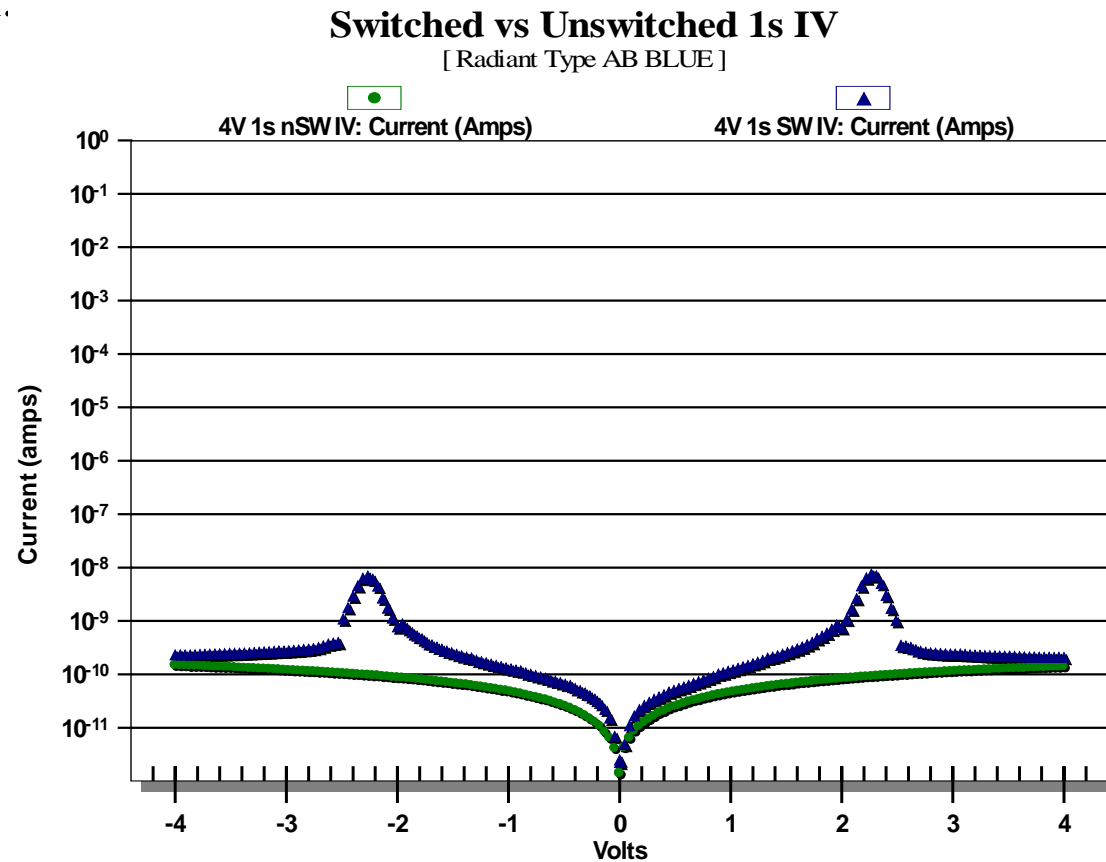


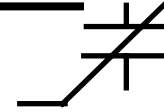
The red line indicates the period during which the leakage through the sample is measured after a soak period.

- The IV, or Current vs Voltage, test is a series of leakage tests executed over the voltage profile used for the traditional hysteresis loop.
- It is necessary because resistive leakage is not always linear!

# Hysteresis in Leakage

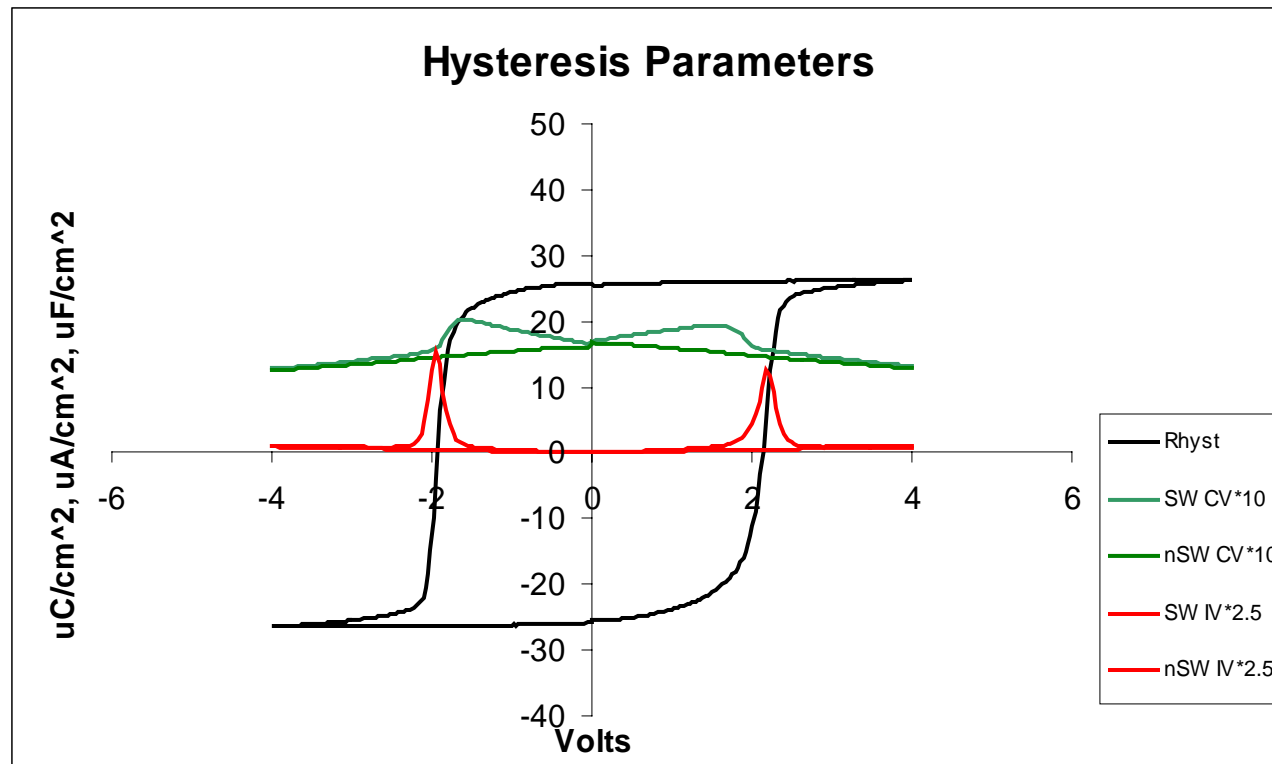
- Leakage in ferroelectric materials does not have to be linear.
- Leakage can have its own hysteresis modulated by remanent polarization.





# Leakage vs CV vs Remanent Polarization

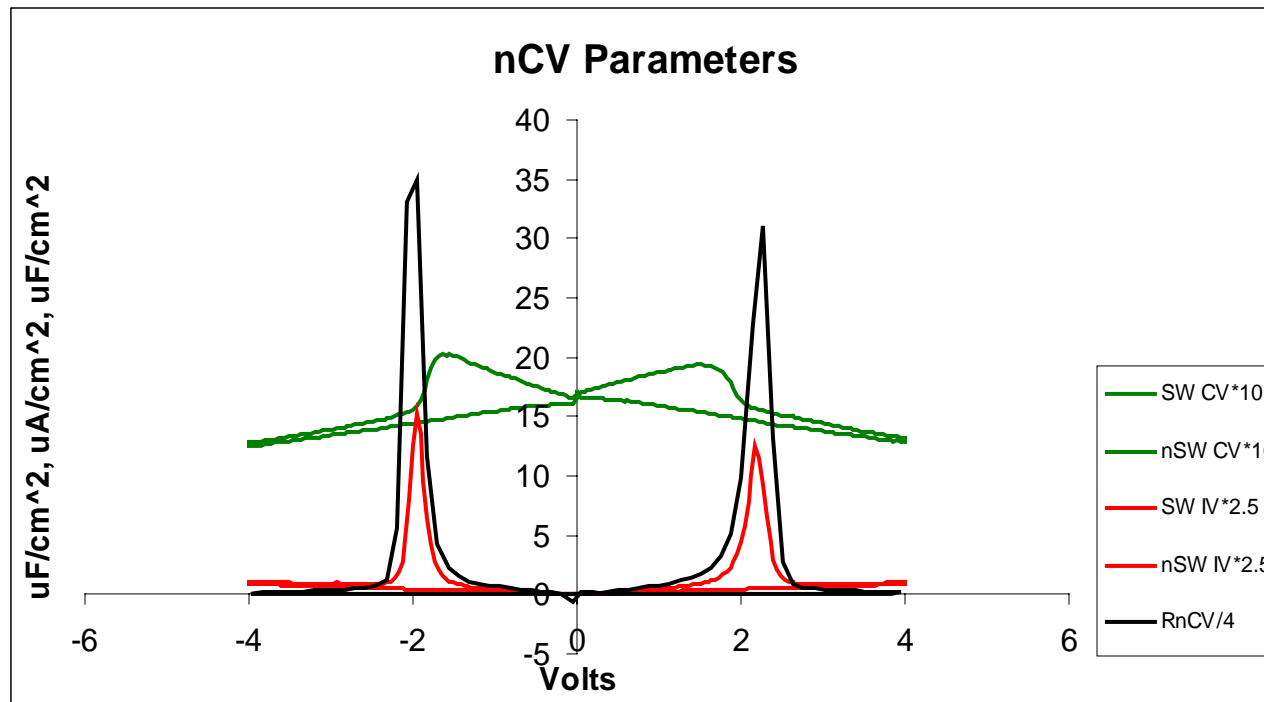
- Are the remanent polarization, IV, and CV related? YES!

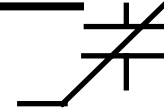




# Leakage vs CV vs Remanent Polarization

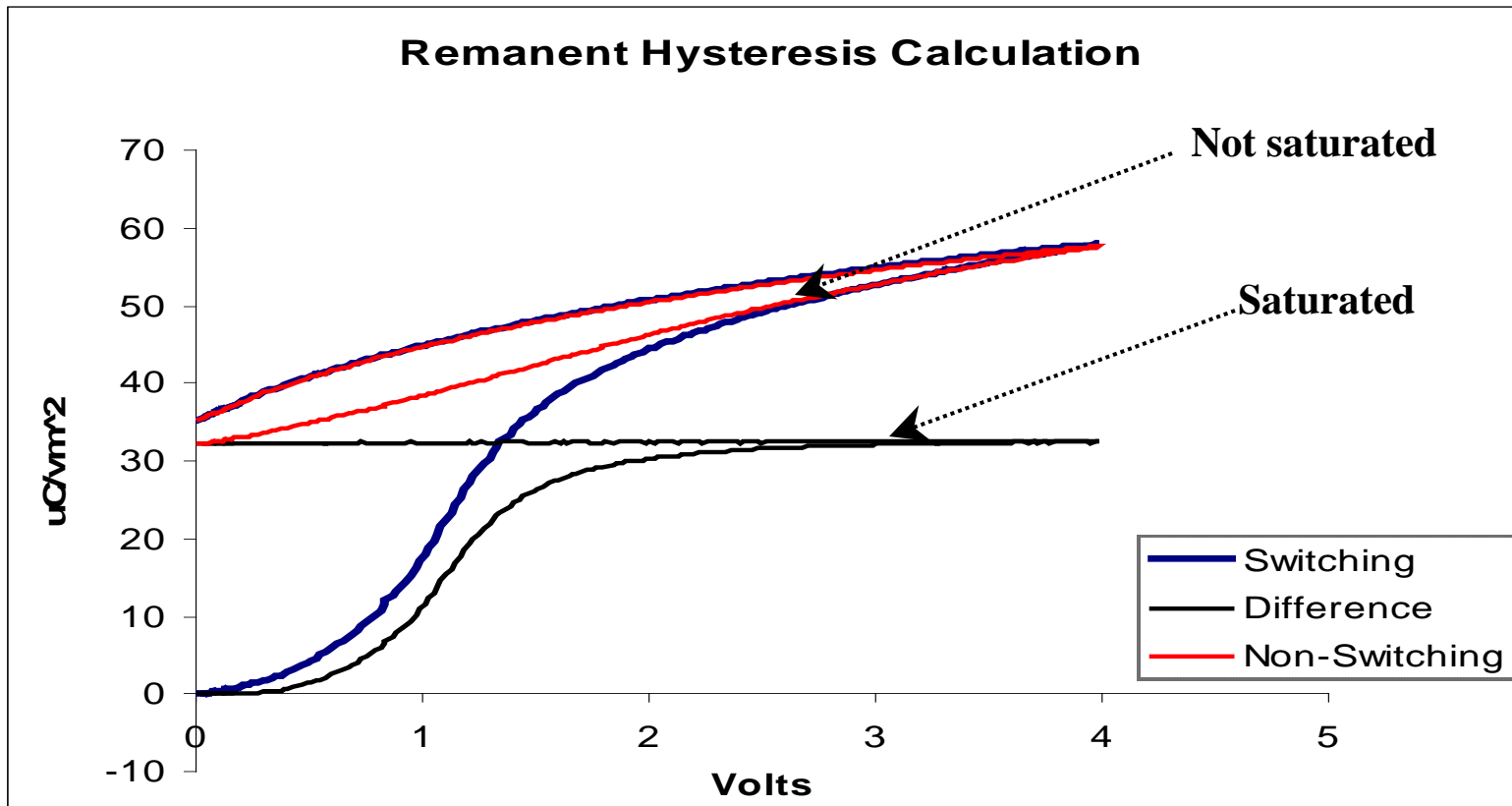
- The derivative of the remanent polarization makes the relationships clear.





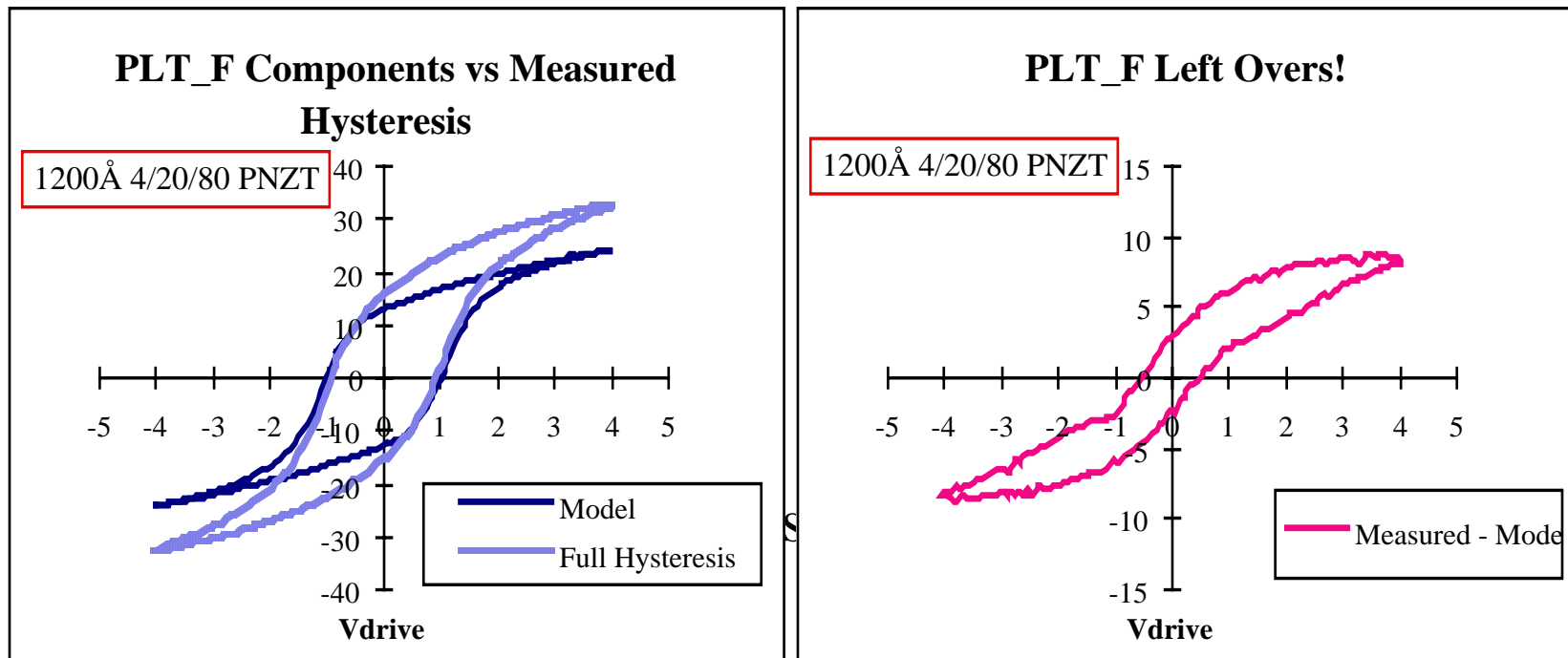
# The Gap

- If remanent polarization saturates nicely, why is the full loop (both switching and non-switching) open at the end?

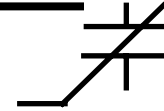


# Something Left Over

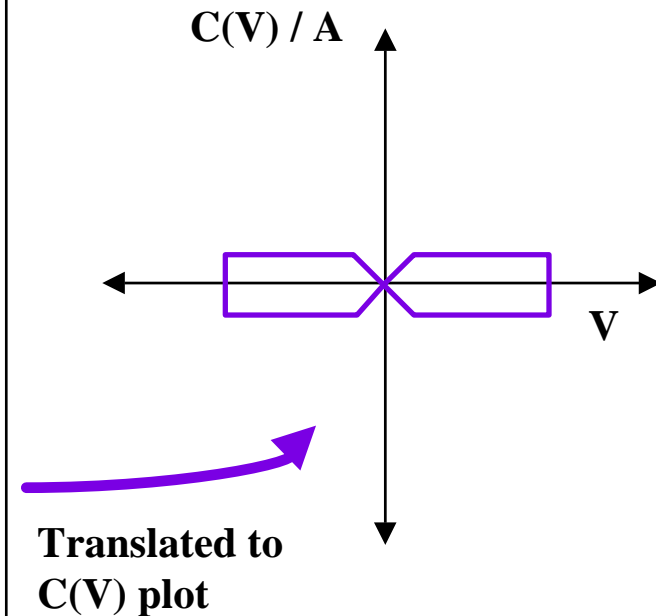
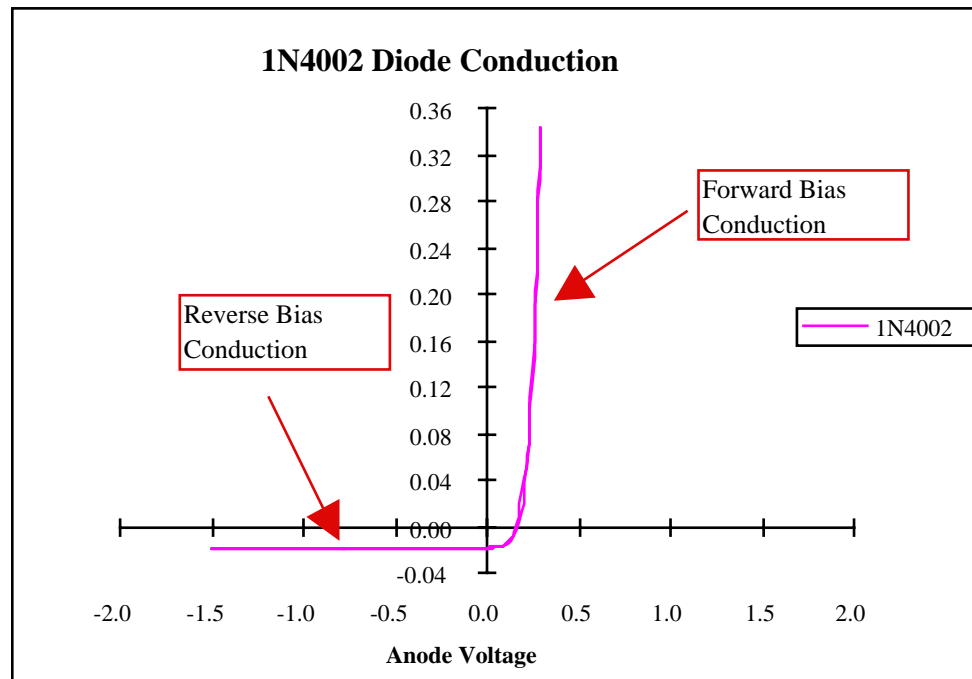
If we measure the remanent polarization, small signal capacitance, and leakage and then subtract them from the full loop, something is left over:



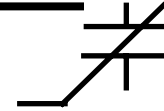
# Reversed Bias Diodes



- A platinum electrode based capacitor has two opposing diodes at the ferroelectric/platinum interface, one of which is always turned off.

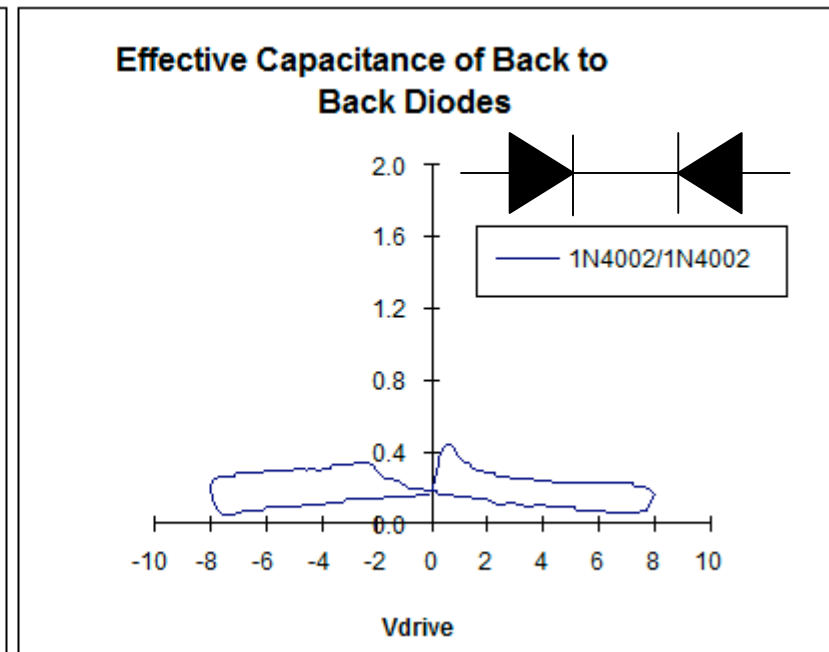
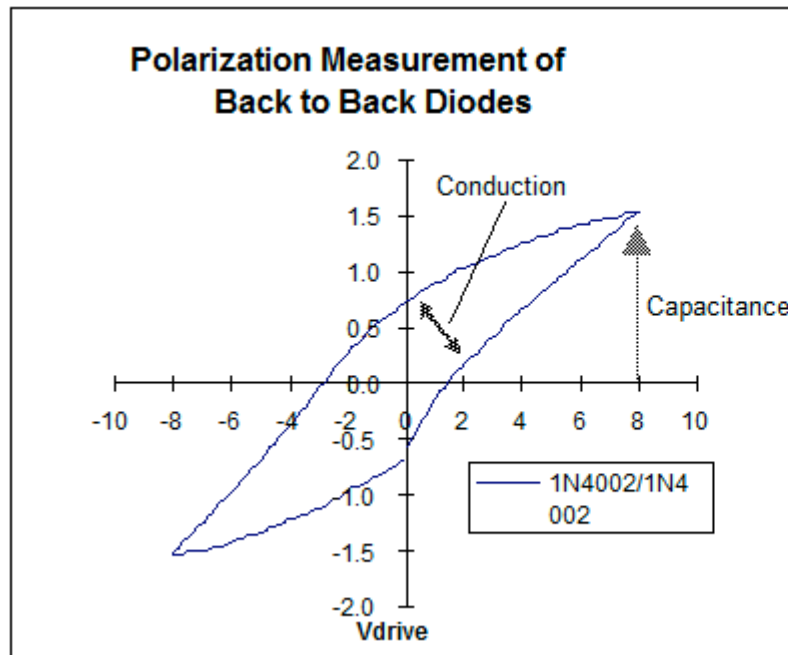


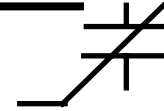
- In reverse bias, a diode has a constant current independent of voltage. *This makes a “bow tie” on the  $nCV$  plot.*



# Reversed Bias Diodes

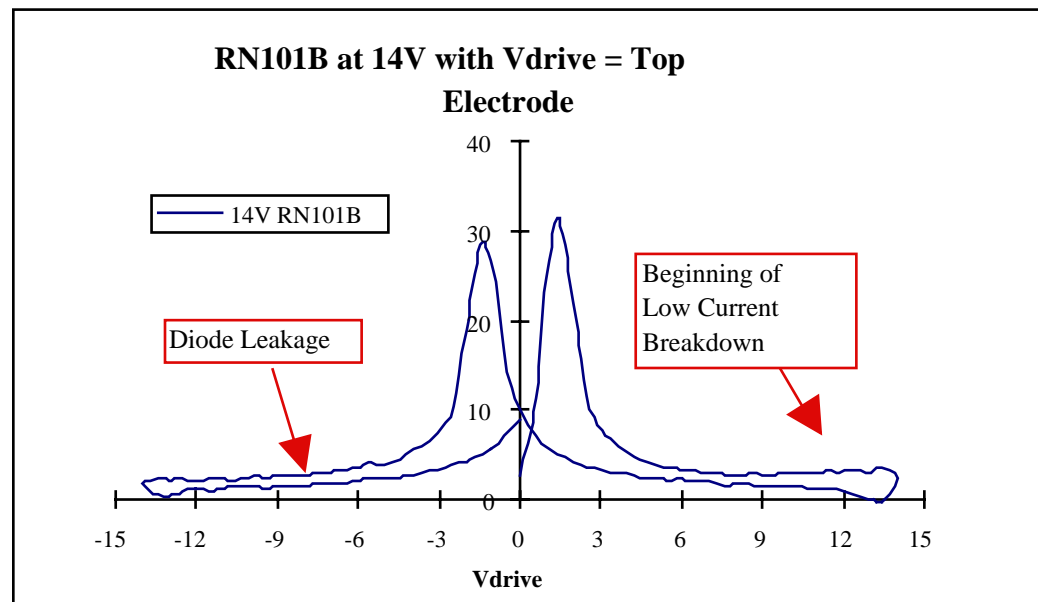
- A pair of back to back diodes have a unique signature on a virtual ground test system which uses a triangular drive voltage.





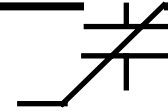
# Reversed Bias Diode Breakdown

- The derivative of a polarization hysteresis loop clearly shows the diode reverse-biased leakage if it is present.



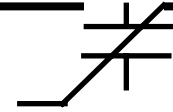
- The leakage of diode reverse-biased breakdown is marked by exponentially increasing current. This produces a “trumpet flare” instead of the “X” of linear leakage.

# The Components



- Remanent polarization
- Linear small signal capacitance (dielectric constant)
- Nonlinear small signal capacitance (dielectric constant)
- Hysteretic small signal capacitance (remanent polarization modulation)
- Linear resistive leakage
- Hysteretic resistive leakage
- Electrode diode reverse-biased leakage
- Electrode diode reverse-biased exponential breakdown

All of these components are visible in the derivative of the polarization hysteresis loop!

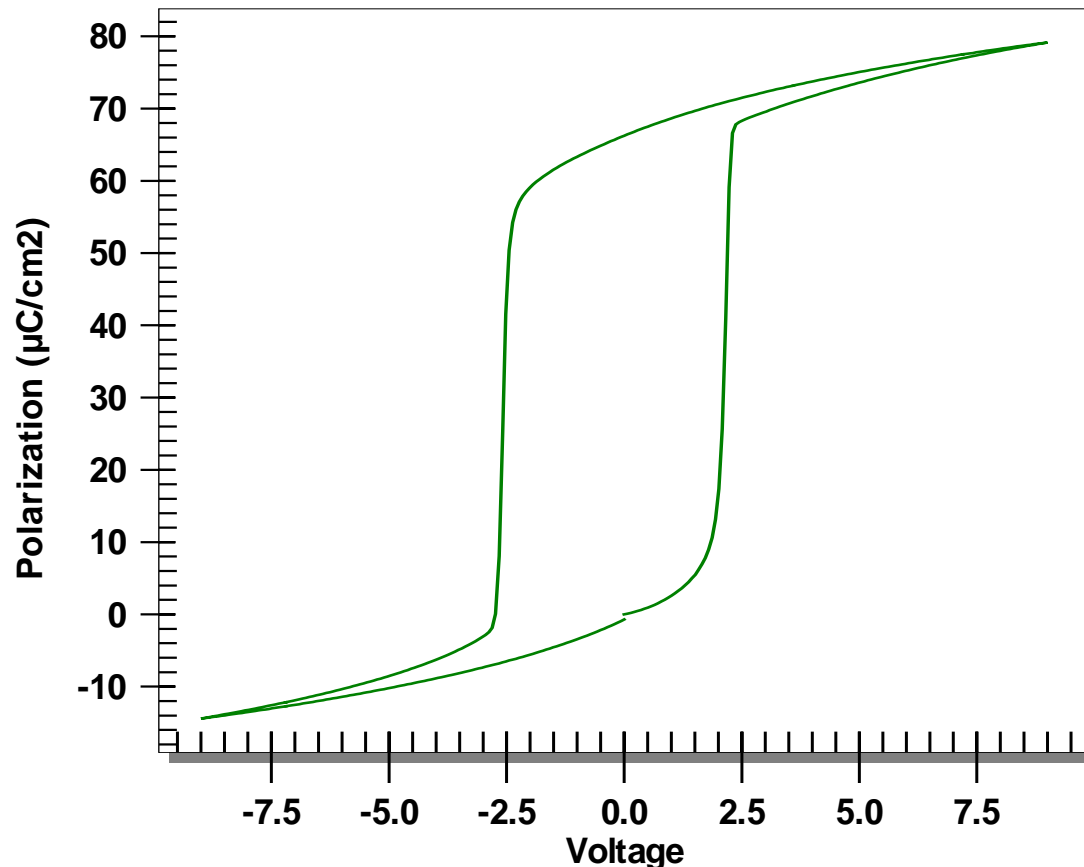


# What is this?

Let's analyze some capacitors!



# An Excellent Hysteresis Loop

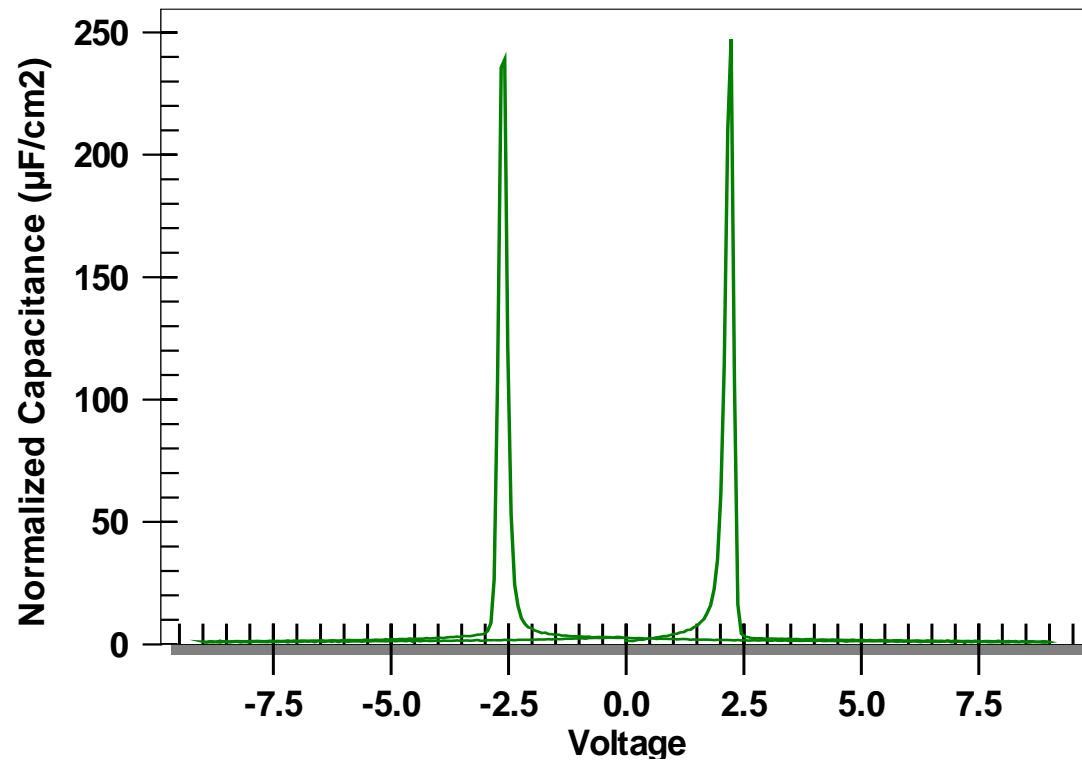


- The nearly “perfect” loop. 20/80 PZT on platinum.

# An Excellent Hysteresis Loop

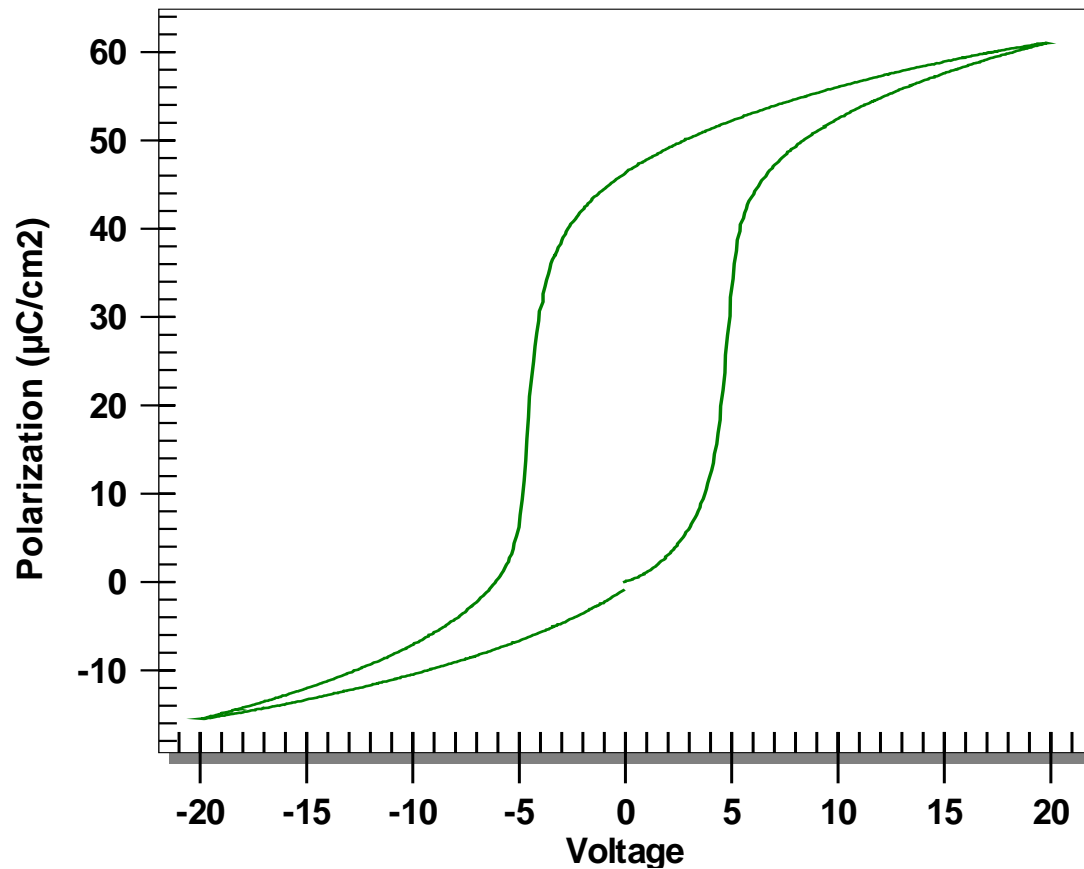
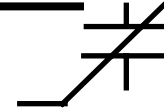
## 20/80 PZT on Platinum

[ 0.26u thick ]



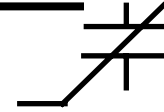
- The 20/80 PZT on platinum is so square that the instantaneous capacitance increases by x250 or more during switching.

# What is this?

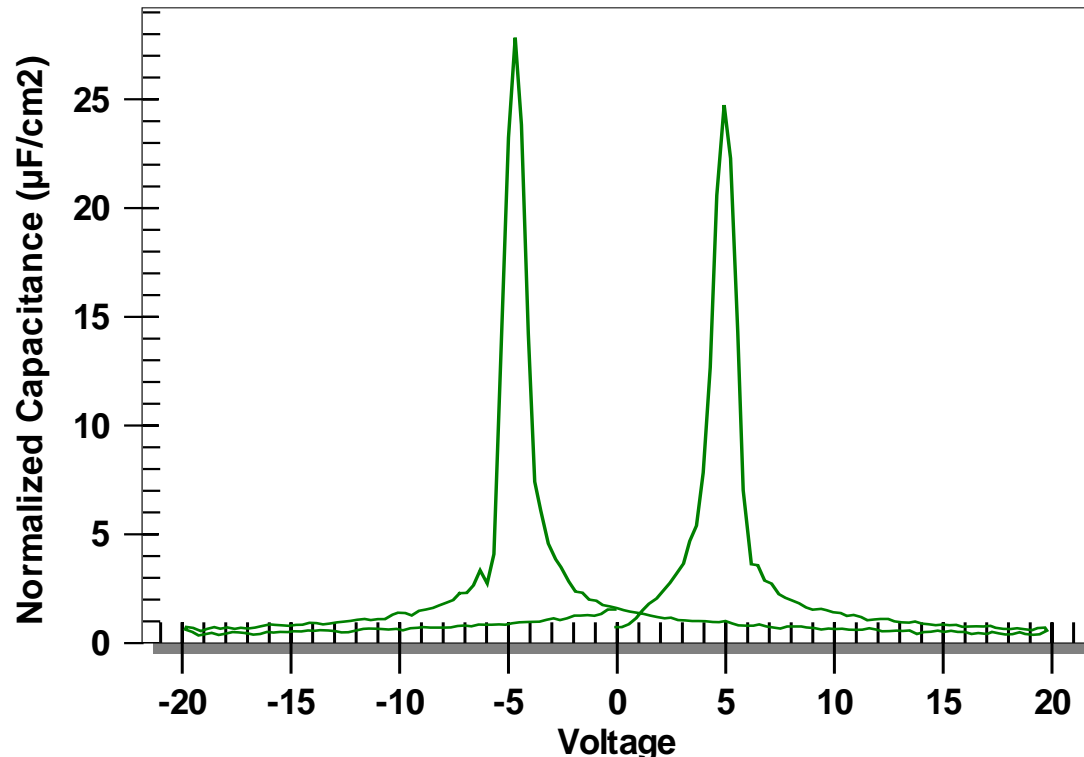


- Is this loop as good as the previous loop? Yes! It is 4/20/80 PNZT, a different composition from 20/80 PZT. So, it has a different shape.

# What is this?

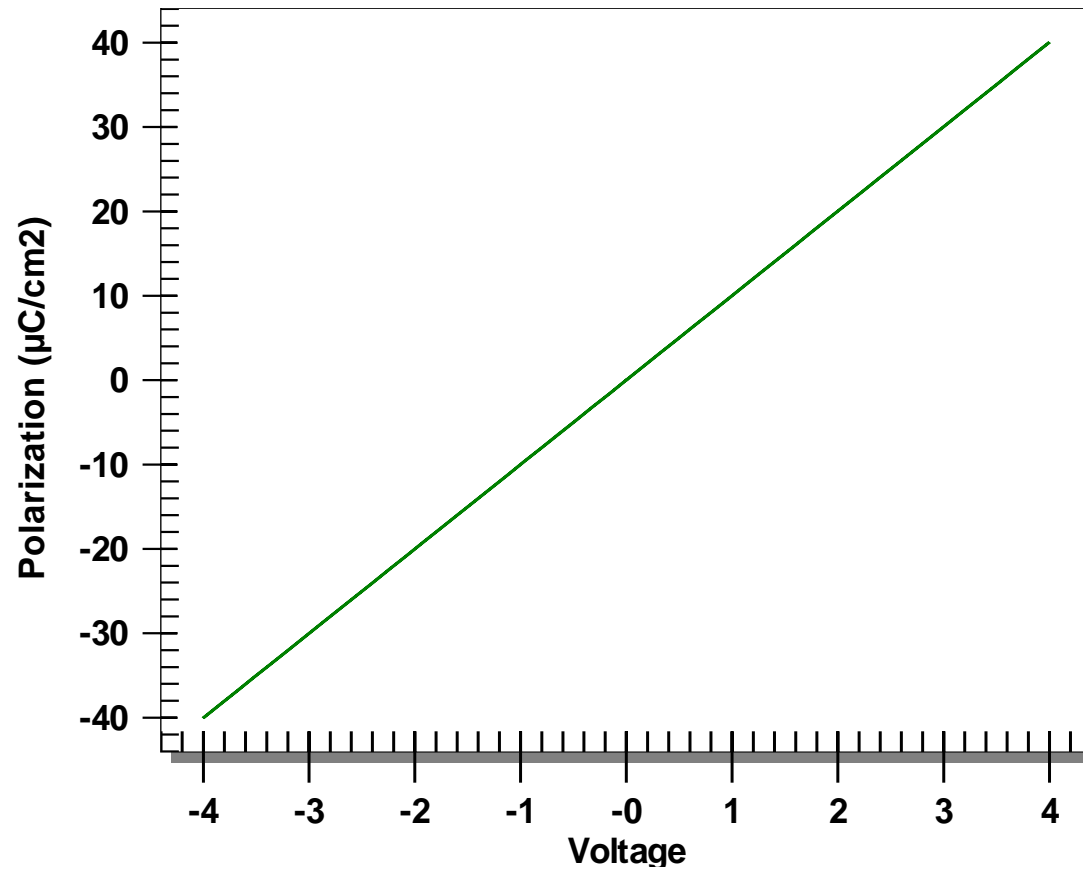
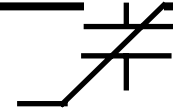


**4/20/80 PNZT**  
[ 1u thick ]



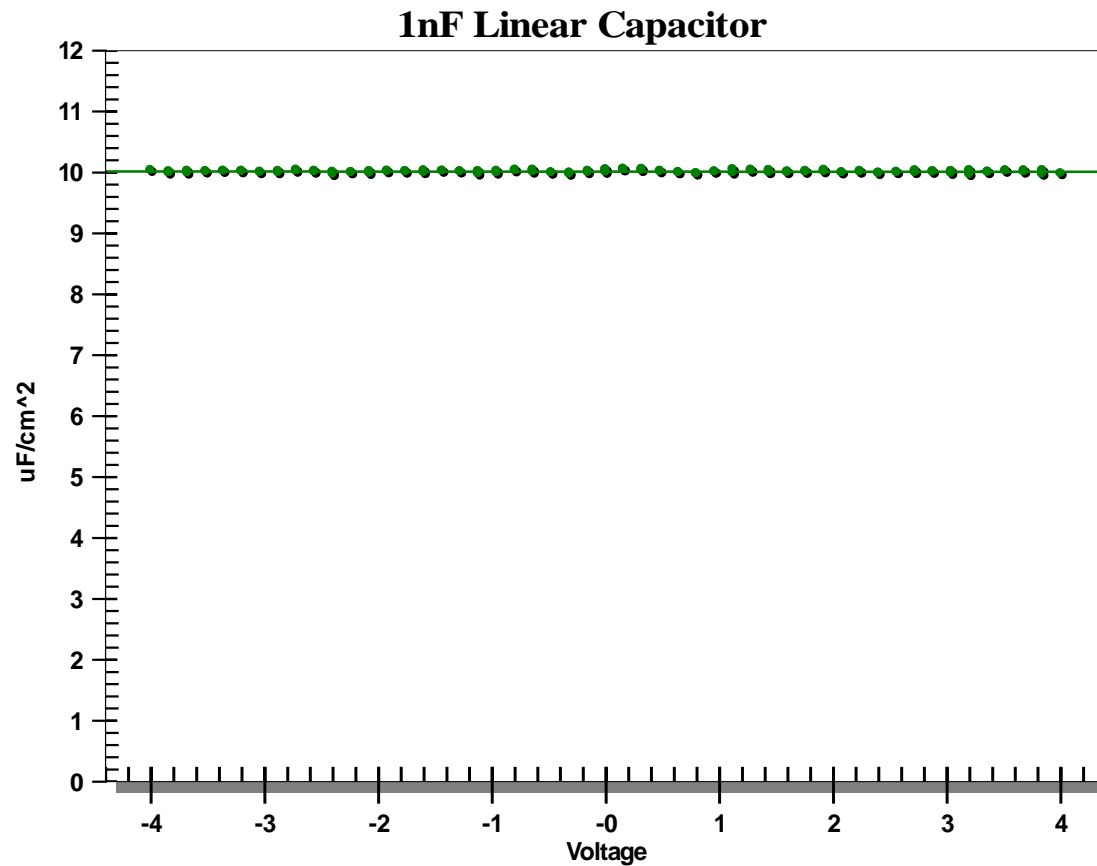
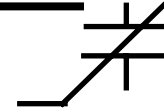
- This loop is good for 4/20/80 PNZT. Note the extra “diode” leakage in the tails that make the saturated tips of the loop open up.

# What is this?



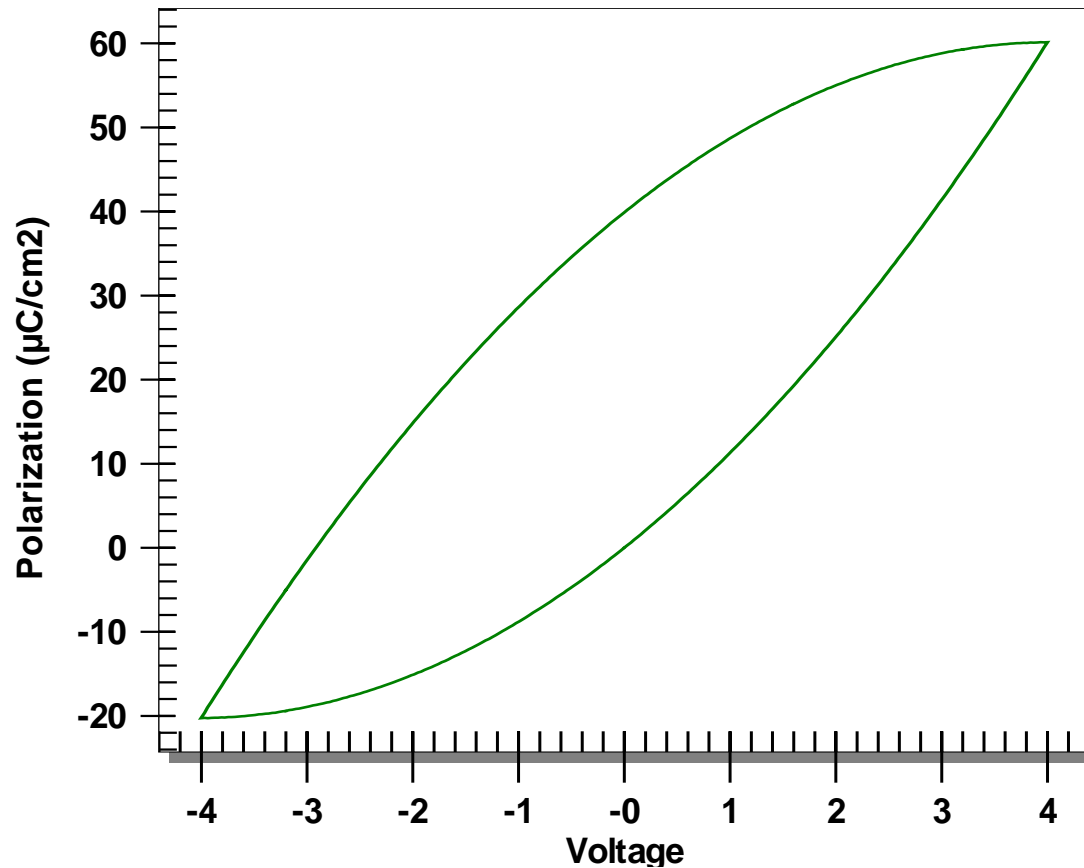
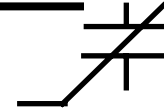
- A linear capacitor.

# What is this?



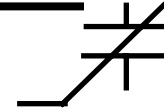
- A linear capacitor. In this measurement, it has a capacitance density of  $10\mu\text{F}/\text{cm}^2$ .

# A Harder One

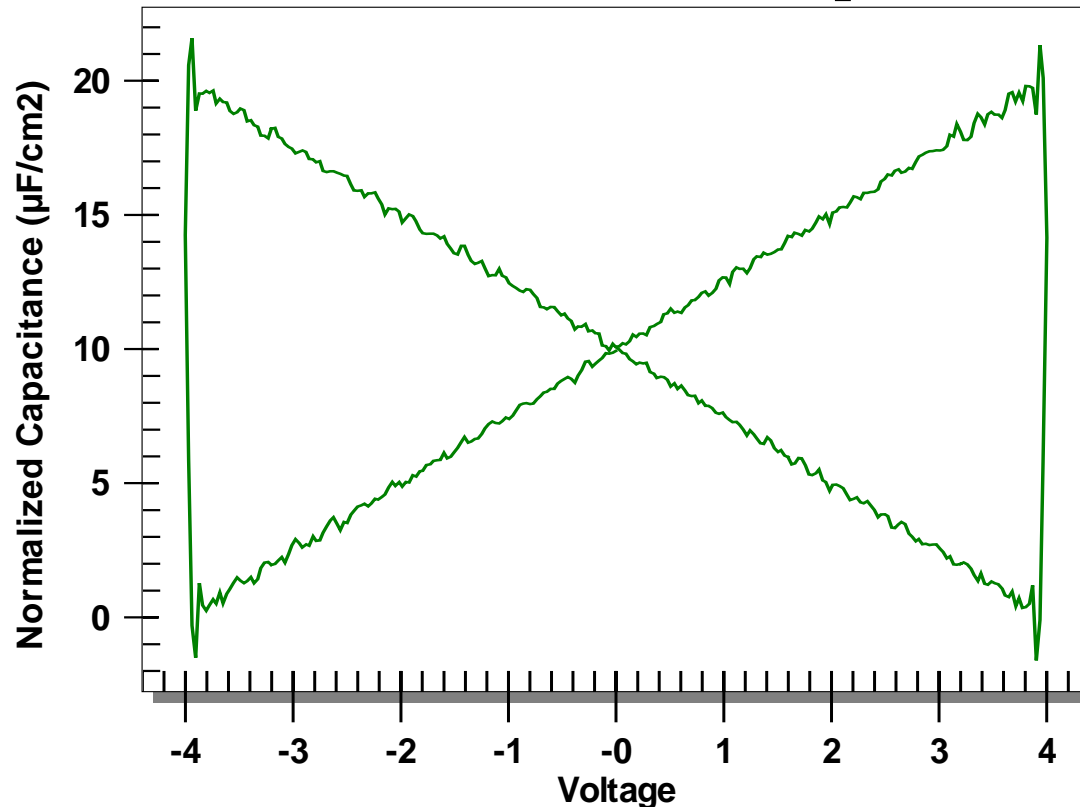


- Quite a few papers include loops that look like this.

# A Harder One



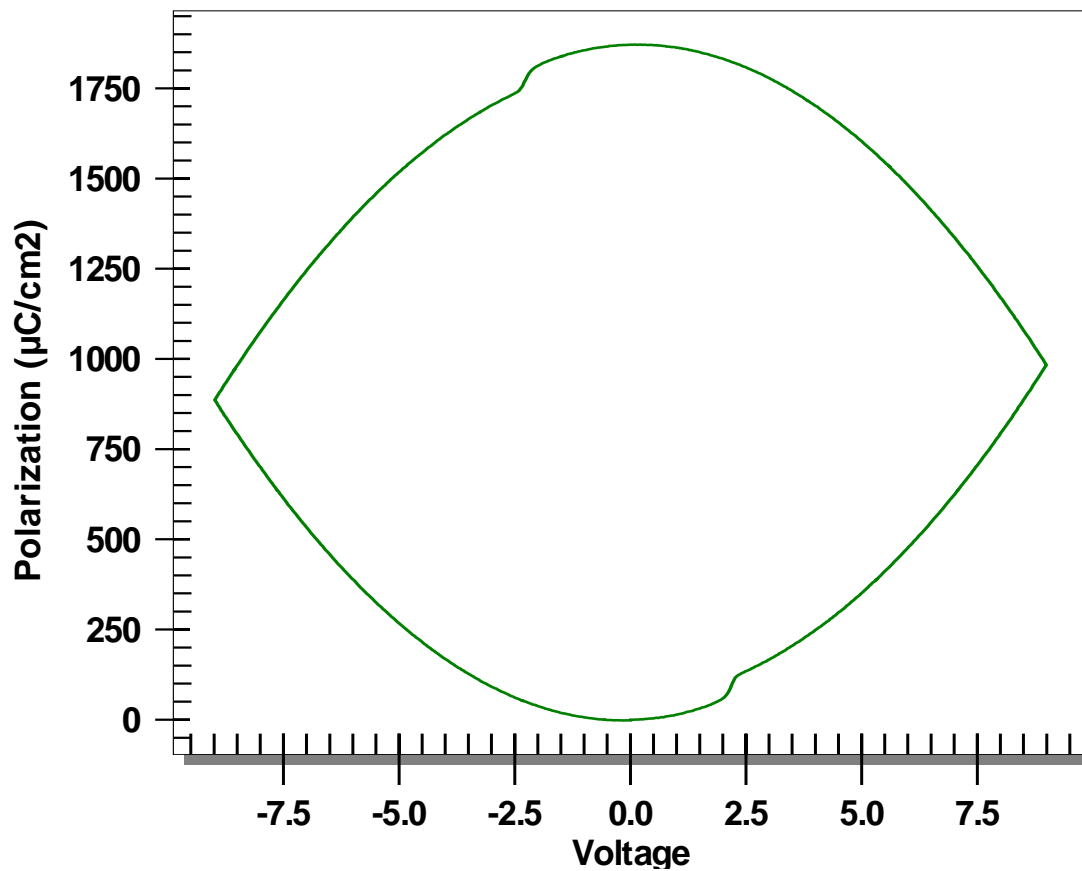
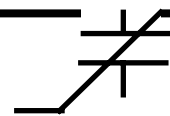
Linear Resistor || Linear Capacitor



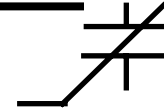
- It is *only* a resistor and a linear capacitor in parallel.



# Is this Ferroelectric?

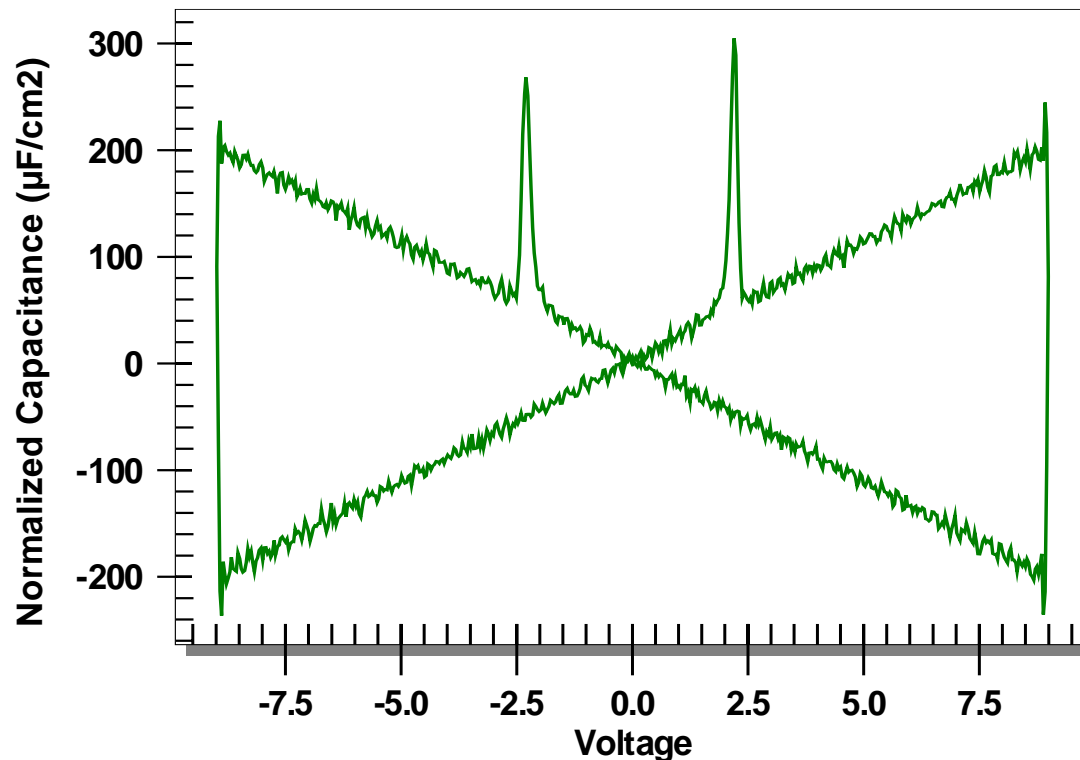


# Is this Ferroelectric?



## Ferroelectric Capacitor || Linear Resistor

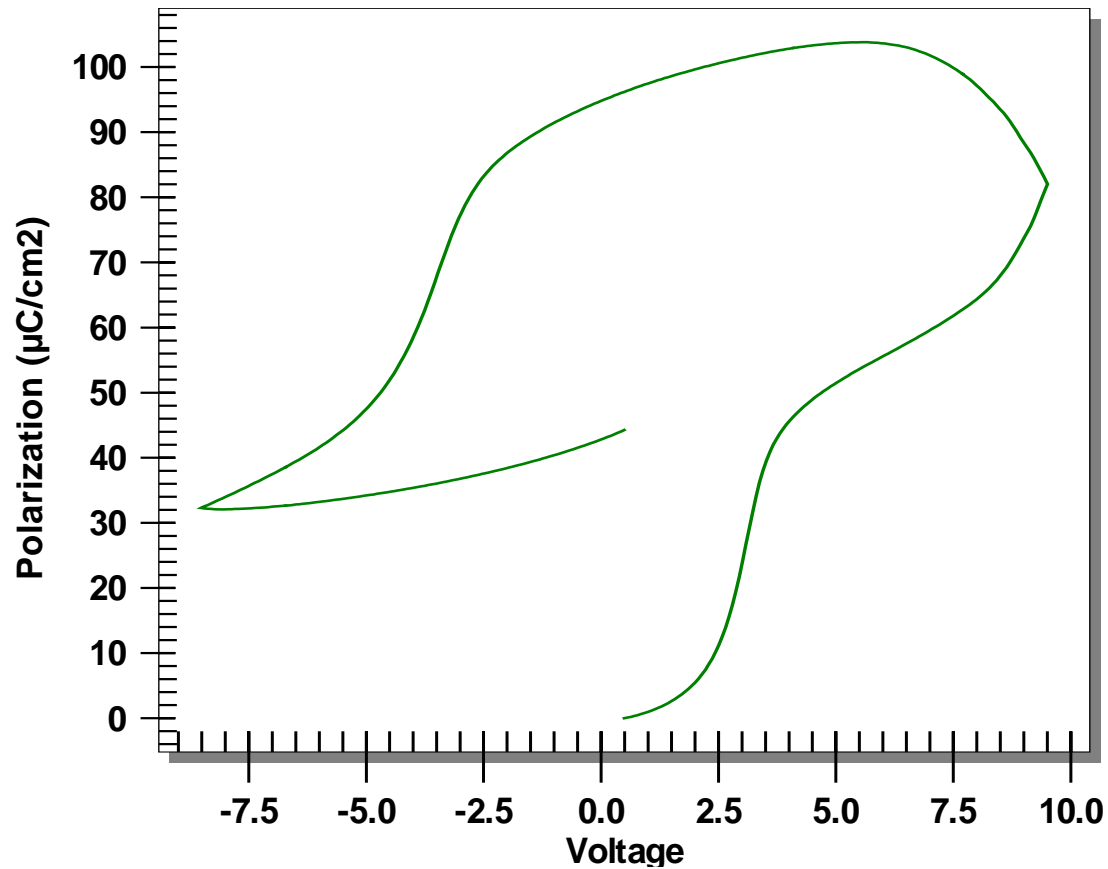
[ Test Period = 2 seconds ]



- Yes, it is! See the ferroelectric switching peaks sticking out of the resistor “X”.

*Radiant Technologies, Inc.*

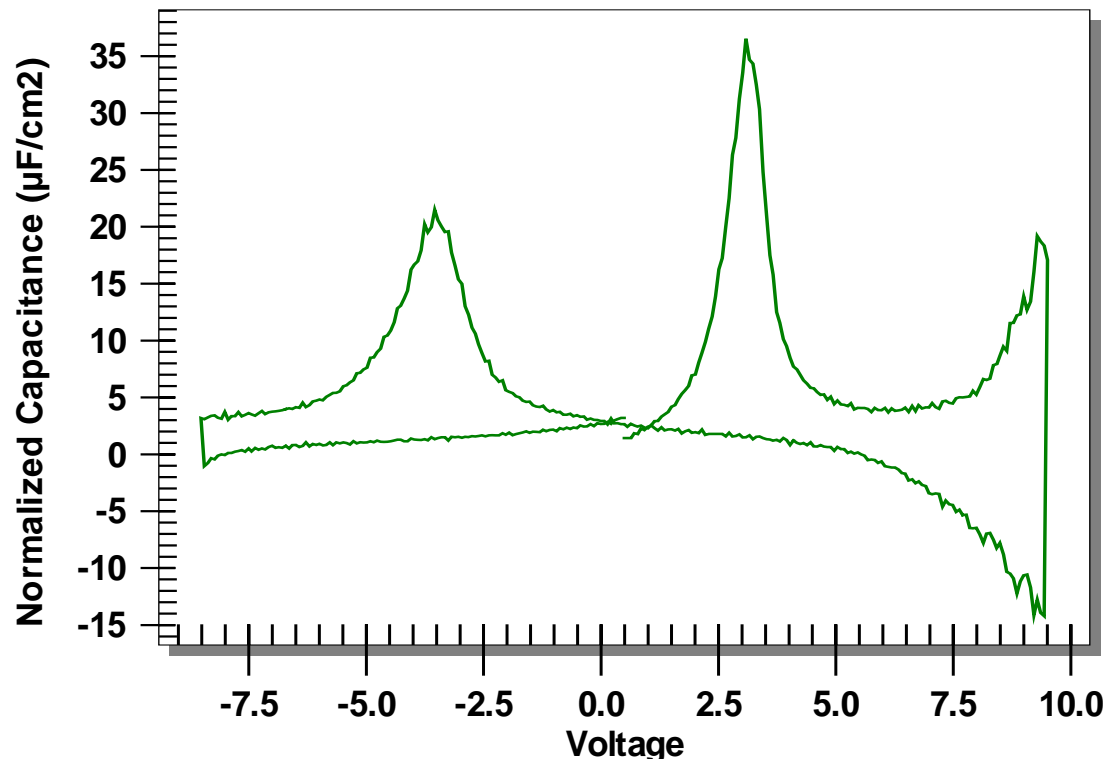
# What Happened Here?



# What Happened Here?

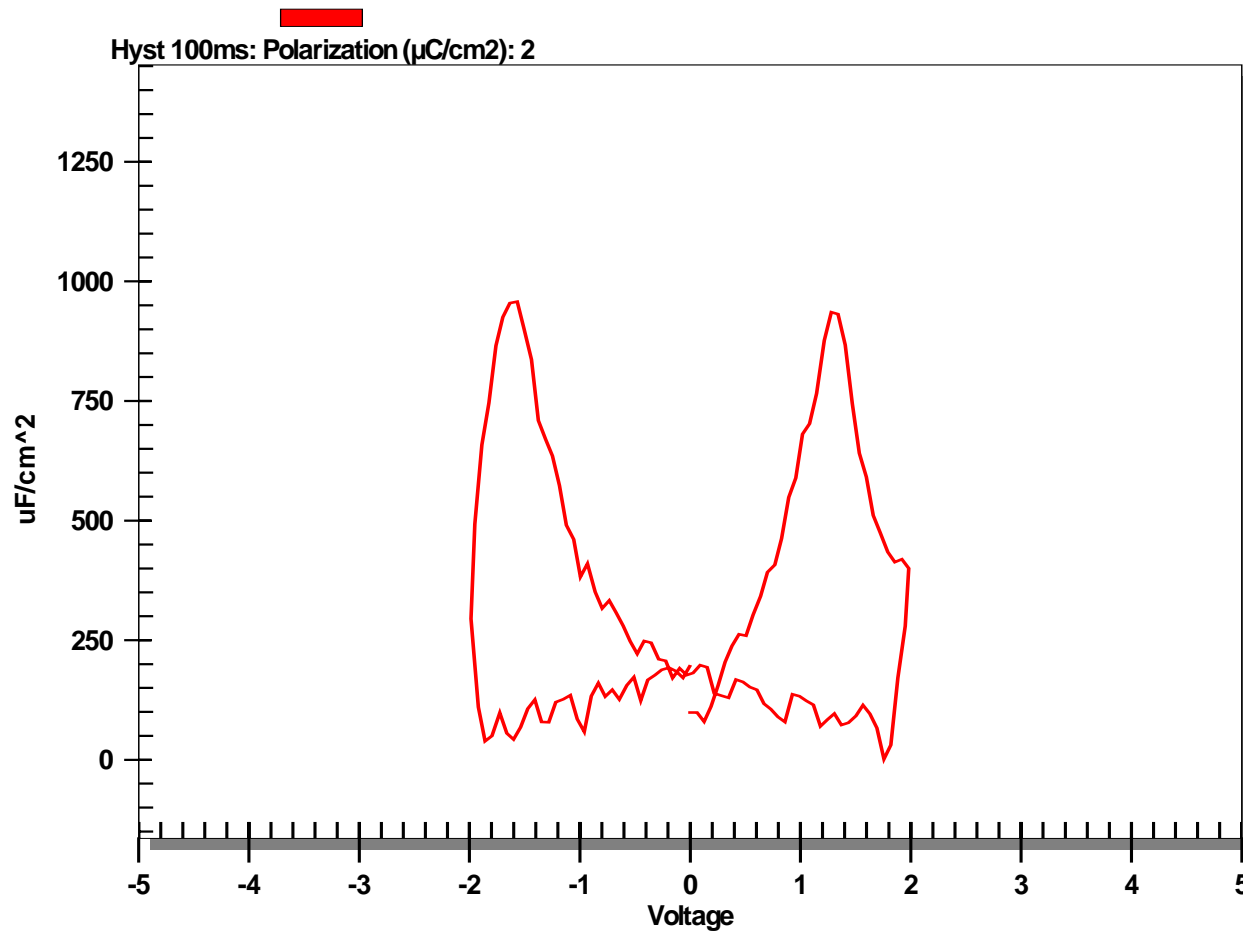
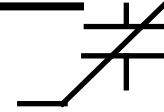
## PZT on Nickel Lanthanate - 300ms Period

[ EXP09BQ Rev A ]



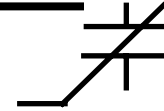
- Different electrodes on each interface means a different switching characteristic with direction. No linear leakage but classic back-to-back diode leakage. Surface diode breakdown at one of the electrode/ferroelectric interfaces.

# Gotcha!

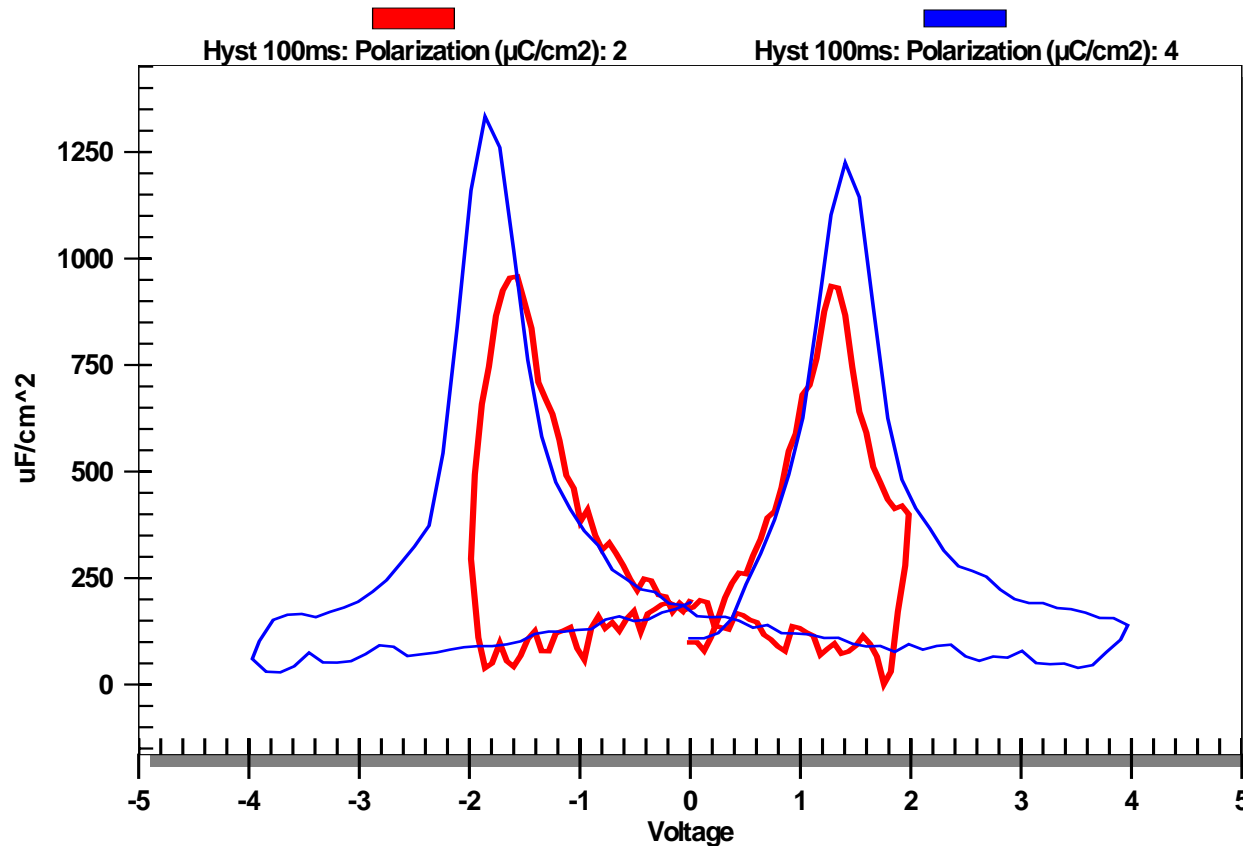


- What is this??? Is it some kind of breakdown???

# Partial Switching!

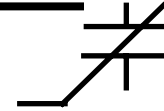


## Nested Loops [LSCO/PNAT/LSCO]

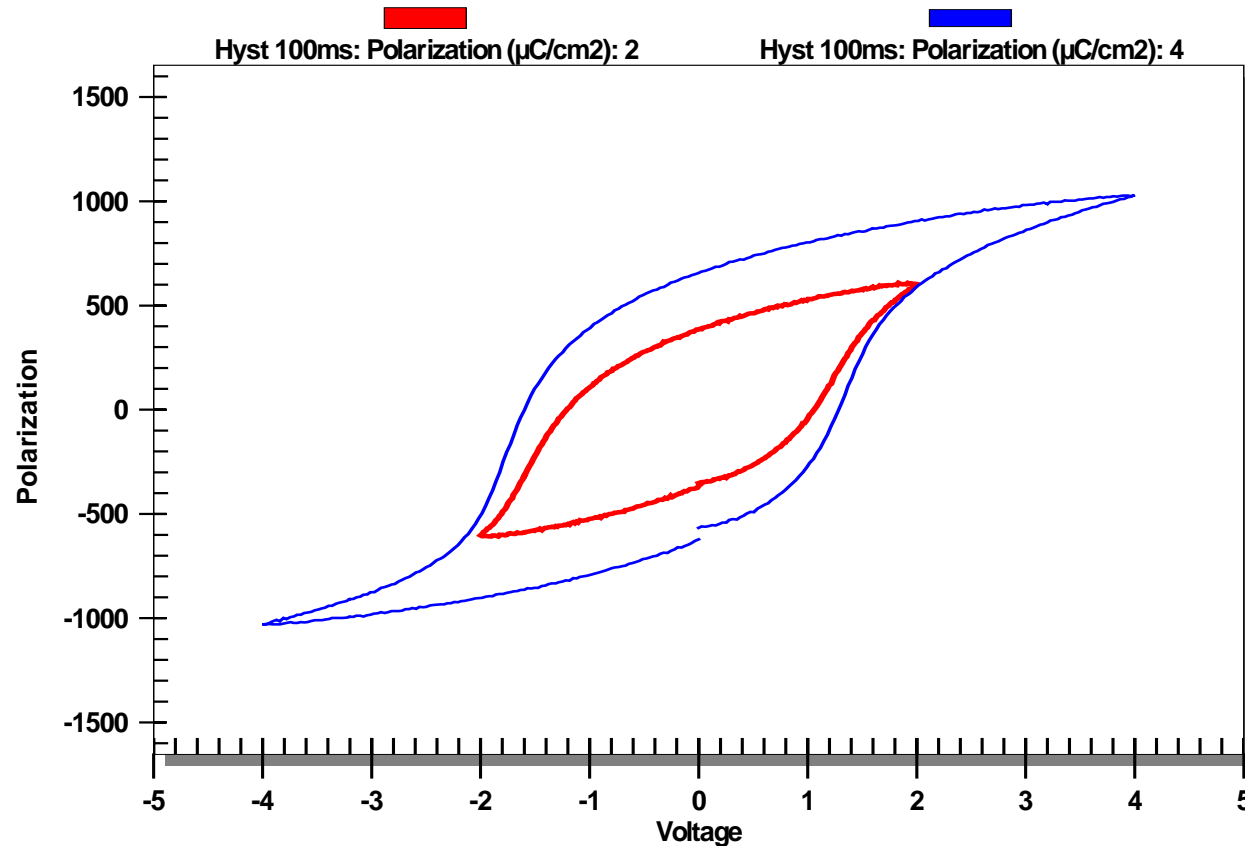


- It is a sub-saturated loop which can sometimes look like breakdown.

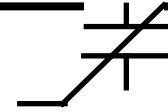
# Partial Switching!



## Nested Loops [LSCO/PNZT/LSCO]



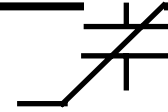
- Here are the hysteresis loops.



# Triangle Wave

- All of the modeling described above is dependent upon using a triangle wave to stimulate the sample.
- $\Delta V / \Delta t$  is constant.
  - $nCV = \Delta Q / \Delta V$
  - $I = \Delta Q / \Delta t \approx \Delta Q / k \Delta V = k \times nCV$





# Conclusion of Components

- Geometry is everything, well almost.
- The ferroelectric hysteresis loop may be broken down into independent components.
- The mathematical derivative of the PE loop is a tool that allows identification by inspection of the components contributing to the response of the sample.
- Practice makes perfect.